PTY, LTD

ACN 010 943 905 ABN 56 010 943 905

P.O. Box 413 Earlyille Q 4870

6 Neptune Court Mt. Sheridan Q 4868 Ph. (07) 4036 1690 FAX (07) 4036 4307 Mobile 0408 770 394

Email: jimpapas@westnet.com.au

June 27, 2011

1208 L01

The Chief Executive Cairns Regional Council P.O. Box 359, CAIRNS Qld. 4870

Attn. Mr. L. Rankine

Dear Sir,



RE: REQUEST FOR FURTHER INFORMATION FOR OPERATIONAL WORKS FOR OCEAN BREEZE ESTATE STAGE 4 AT 905L COOYA BEACH ROAD BOONIE DOON (Your Ref. 8/10/44 (2449462)

We refer to your Request for Further Information (RFI) dated January 18, 2010.

BACKGROUND

This development property has been sold. We act on behalf of the new owners Jonpa Pty. Ltd in conjunction with Briley Consultants Pty. Ltd. We advise Council that we have been appointed as designers of this project and all future correspondence should be directed to us. The original application for Stage 4A was lodged by the former consultant, Sinclair Knight Mertz (SKM). SKM are no longer associated with the project.

For various reasons we are unable to access the design calculations, drawings and other data on which the original application was based. Therefore our response to Council's RFI is based on such information that is available on the public record or that we have developed ourselves. We have redrawn the engineering drawings to reflect our responses contained in this letter. A full set of the revised engineering drawings is attached as Appendix A.

On this basis, we respond to Council's RFI as follows:

Item 1 "Confirm all lots are immune to a 1 in 100 year ARI event."

RESPONSE

Based on the stormwater drainage calculations shown on Dwg 1208 C13, we conclude that all proposed lots in Stage 4A of Ocean Breeze Estate are above the inundation level caused by a rainfall event of ARI 100 years.

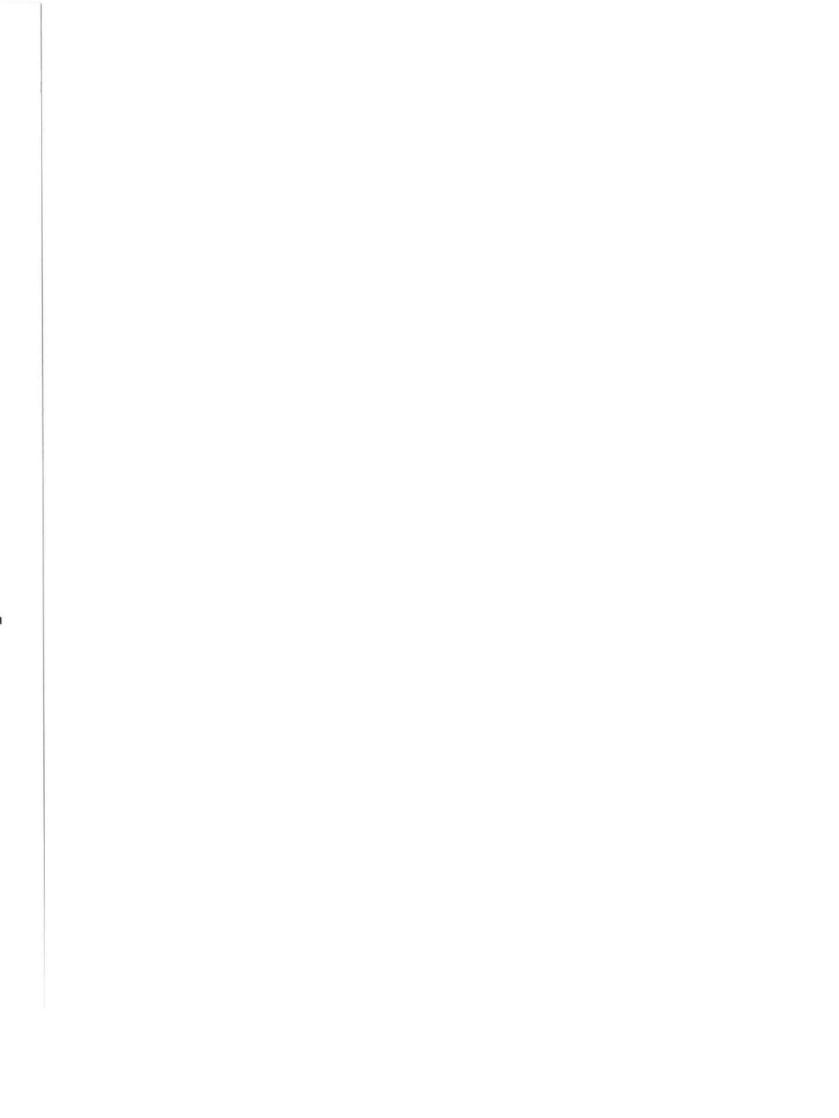
Item 2 "Extended lengths of infrastructure crossing under roadways are not supported by Council.

Please amend stormwater line 3/12 to 2/12 such that the shortest possible crossing length is achieved.

An additional manhole may be required."

RESPONSE

We have redesigned the stormwater drainage layout, which has substantially reduced the length of stormwater drainage pipework under roadways. The revised layout is shown on Dwg 1208 C04.



PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

Item 3 "Confirm all sub-catchments time of concentrations are 15 minutes."

RESPONSE

We refer Council to the Queensland Urban Drainage Manual (QUDM) Table 4.06.1 "Recommended standard inlet times" which notes that the standard inlet time for an urban residential catchment where the average slope of land at the top of the catchment is up to 3% is 15 minutes. Therefore this is the appropriate time of concentration for these catchments.

Item 4 "Confirm flows width in the kerb and channel (Column 15, Drawing CB22504-C-16) for a 5 year flood event are in accordance with the maximum allowable flow widths identified in the Queensland Urban Drainage Manual."

RESPONSE

The QUDM Table 7.04.1 Roadway flow widths and depth limitations (longitudinal drainage) indicates that for both Road B and H the permitted flow width is "Full pavement width with zero depth at crown". Our revised design achieves this outcome as shown on Dwg 1208 C13.

Item 5 "Undertake a drainage study of the site to determine the drainage impacts on upstream and downstream properties and the mitigation measures required to minimise such impacts. In particular, the study must address the following:

- a. The contributing internal and external catchment boundaries;
- The extent of the 100 year ARI flood event in relation to the site both pre and post development;
- c. Primary and secondary flow paths for the 5 and 100 year ARI flood events;
- d. Identify the need and tenure for flood detention areas to ensure a no worsening impact on downstream properties for the entire development;
- e. Information on the proposed works and any impacts proposed at the drainage outlet from the proposed development.
- f. Lawful point of discharge.

The study must be endorsed by the Chief Executive Officer prior to the issue of a development permit for operational works."

RESPONSE

We note that the Amended Decision Notice Approval dated September 7, 2007 on which this application is based does not impose any conditions with respect to ensuring a no worsening impact on downstream properties nor do they require determination of the extent of flooding for pre and post development. Therefore, we do not believe that we are obliged to provide any such information and we have not responded to Items b and d above.

We have attached our Overall Stormwater Drainage Plan Dwg 1208 OA Stm as Appendix B, which shows:

- a. The contributing internal and external catchment boundaries;
 - c. Primary and secondary flow paths for the 5 and 100 year ARI flood events;
- iii) f. The lawful points of discharge

With respect to Item e above, we believe that such information is a matter of detailed design, which we have not undertaken at this time. We will be pleased to provide such data at the appropriate time in conjunction with the application for a Development Permit for Operational Works associated with the particular drainage outlet.

Item 6 "Water

Identify on the drawing the clearances (horizontal and vertical) between the proposed water main pipes, and other services to verify compliance with WSA 03-2002, Table 4.1 at the following points: a. At the intersection between Road H and Road B, where:

• The proposed ø50mm uPVC water main crosses the proposed ø450mm stormwater pipe.

PTY. LTD

ACN 010 943 905 ABN 56 010 943 905

The proposed ø100mm uPVC water main crosses the proposed ø375mm stormwater pipe
 b. At Road B in front of Lot 117, where the proposed ø100mm uPVC water main crosses the proposed ø600mm stormwater pipe."

RESPONSE

The stormwater system has been redesigned but we decline to provide this information

Item 7 "The proposed hydrant located in front of Lot 117 is to be relocated such that it is situated in line with the property boundary."

RESPONSE

We have located the fire hydrant to near the end of the existing water main so that it may be used as a flushing point. It will be close to the existing stop valve. Refer to Dwg 1208 C07

Item 8 "Amend Note 1, such that all water mains are on 2.8m alignments from R.P. Boundaries, in accordance with FNQROC Design Guideline Table 06.2."

RESPONSE

On Dwg. 1208 C07 we stipulate that the water main alignment is 2.80m from the RP Boundaries.

Item 9 "Comments on Water Analysis

Water & Waste have reviewed the information provided in support of the above proposed development and have the following observations:

The report only considers Stage 1 and the ultimate development - it does not consider Stage 4A as an interim development. The report needs to be updated to include Stage 4A as an interim stage in addition to consideration of the ultimate development, for that reason Water & Waste was not able to complete a full review of the water reticulation analysis, but make the following comments:

- a. Modelling has adopted the Colebrook-White head loss formula. Although this is not inappropriate, Council requires the use of Hazen Williams head loss formula (per FNQROC Design Guidelines) as a more relevant approach for water reticulation analysis. The Hazen Williams "C" values stated in FNQROC shall apply.
- b. It is noted that an average daily usage of 700Llperson/day has been adopted. FNQROC requirements are for an average daily consumption of 500Llperson/day, which has also been adopted for Division 10. The modelling and report needs to reflect an average daily consumption of 500L/person/day.
- Confirm the operating water level adopted in the new Cooya Beach Reservoir for the scenarios modelled.
- d. Advise the future stage of the development requiring provision of the duplicate 0150mm main from the Cooya Beach Reservoir to connect to the new 0200mm main in Cooya Beach Road shown in Dwg. No. CF22501-F-02 (Amdt B)."

RESPONSE

We attach our Water Supply Report as Appendix C, which incorporates the following:

- Our analysis, which has been done using EPANet program, which in turn uses the Hazen Williams equation together with the appropriate "C" values.
- ii. An average daily consumption of 500 L/person/day has been adopted.
- ii. The new reservoir levels have been adopted. The relevant parameters are noted in our report
- iv. Earlier information contained in SKM's planning clearly indicated that the existing water supply connection to the reservoirs is a 200ø water main. We cannot explain SKM's submitted data for Stage 4A showing a duplicate 150ø water main. We can only suggest that this is an error.

8"			
0 30			
•			
t			
า			
S			
· ·			

ACN 010 943 905 ABN 56 010 943 905

Item 10 "The following existing drop distances have to be amended in accordance with the Standard Drawing S3000-CRC Rev (B)."

RESPONSE

We have redesigned the sewerage reticulation system such that the sewers now comply with these requirements. Refer to Dwg 1208 C06.

Secondary Issues

Item 11 "Amend drawings to provide a 2.0m footpath along the Northern side of Road B and Road H (ie. On the frontage to Lots 114-117).

RESPONSE

The amended drawings show a concrete footpath along the northern side of Juluji Close and Road H.

Item 12 "Amend plans to show a buffer mound to the frontage of Bonnie Doon Road as required by development approval dated 7 September 2007. This may be shown on the landscaping plan to be submitted to Council."

RESPONSE

This matter shall be addressed as part of the landscape plans.

This completes our response to your Information Request. We have addressed each item in your letter and have indicated whether or not we have supplied the requested information. We have supplied most but not all of the requested information and ask for Council to proceed with the assessment of the application.

FURTHER MATTERS

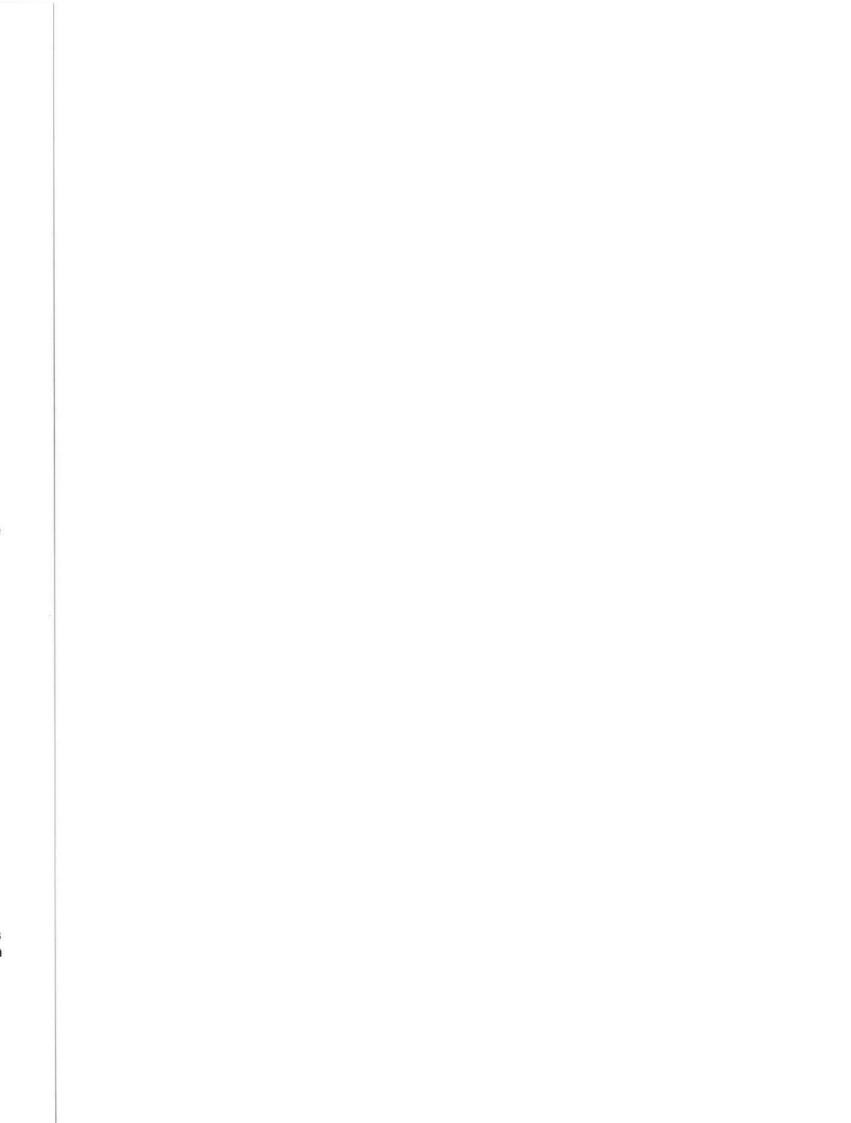
During our design process we noticed two items that in accordance with the provisions of the FNQROC Development Manual we are required to obtain Council's prior approval.

Firstly we draw Council's attention to the longitudinal grade in Road H as shown on Dwg. No. 1280 C09, which is 0.3%. This is a flatter grade than the general permissible grade of 0.5%. We have adopted this grade because we expect that using a grade 0.5% along the entire length of Road H would result in a road level at the northern end of Road H that is about a metre below the existing crown level of Cooya Beach Road. While this may have aesthetic implications it will also cause significant problems with the provision of primary and secondary drainage infrastructure at this location. Therefore, we request that a minimum longitudinal grade of 0.3% be permitted along Road H. The soil profile in the area indicates that the subgrade is predominately sand, which is relatively stable, hence we do not consider that any significant movement of the subgrade is likely, therefore the flatter grade will be satisfactory.

We seek Council's written approval of this proposal.

Secondly we examined our future sewerage options and discovered that it is necessary to install another sewage pump station probably near Lot 246. We attach Dwg 1208 OA Sewer, attached as Appendix D, which shows the future sewer layout. So that excavation may be minimised, we request that Line 27 from Manhole 7/12 to 10/27 be laid at a grade of 1:180. This is permitted by the provisions of the FNQROC Development Manual provided that the sewer is located in flat country and a minimum 20 EDC are serviced. This proposal complies with both these conditions.

We seek Council's written approval for this proposal.



PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

Our Client is anxious to proceed with construction in the near future. To assist our Client in this regard, we are prepared to attend any necessary meeting to discuss these or any other relevant matters to facilitate a prompt resolution and the provision of an Operational Works Permit.

We trust that this is satisfactory, however, if you require further information of if you any queries please do not hesitate to contact the undersigned.

Yours faithfully,

JIM PAPAS DRAFTING PTY. LTD.

JIM PAPAS

Attachments

Appendix A: Cover Sheet plus Dwgs. 1208 C01 to C13 inclusive. (Separate folio)

Appendix B: Dwg 1208 OA Stm.

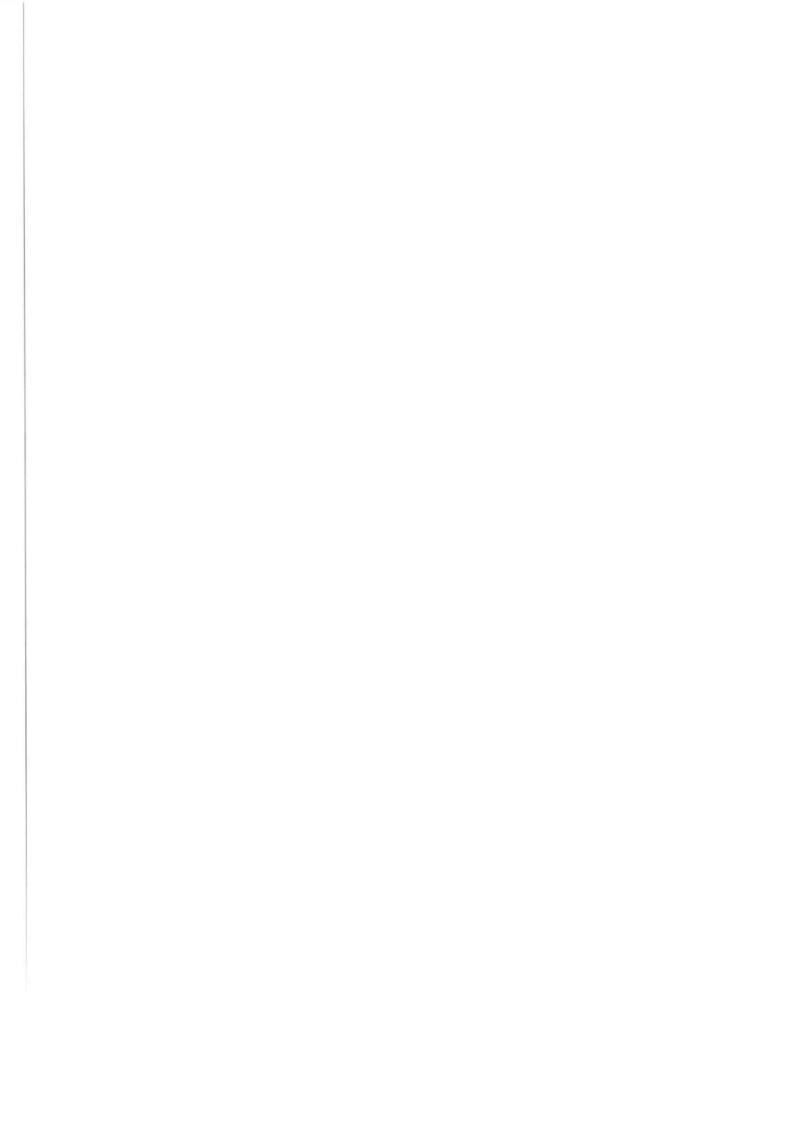
Appendix C: Water Supply Reticulation Report

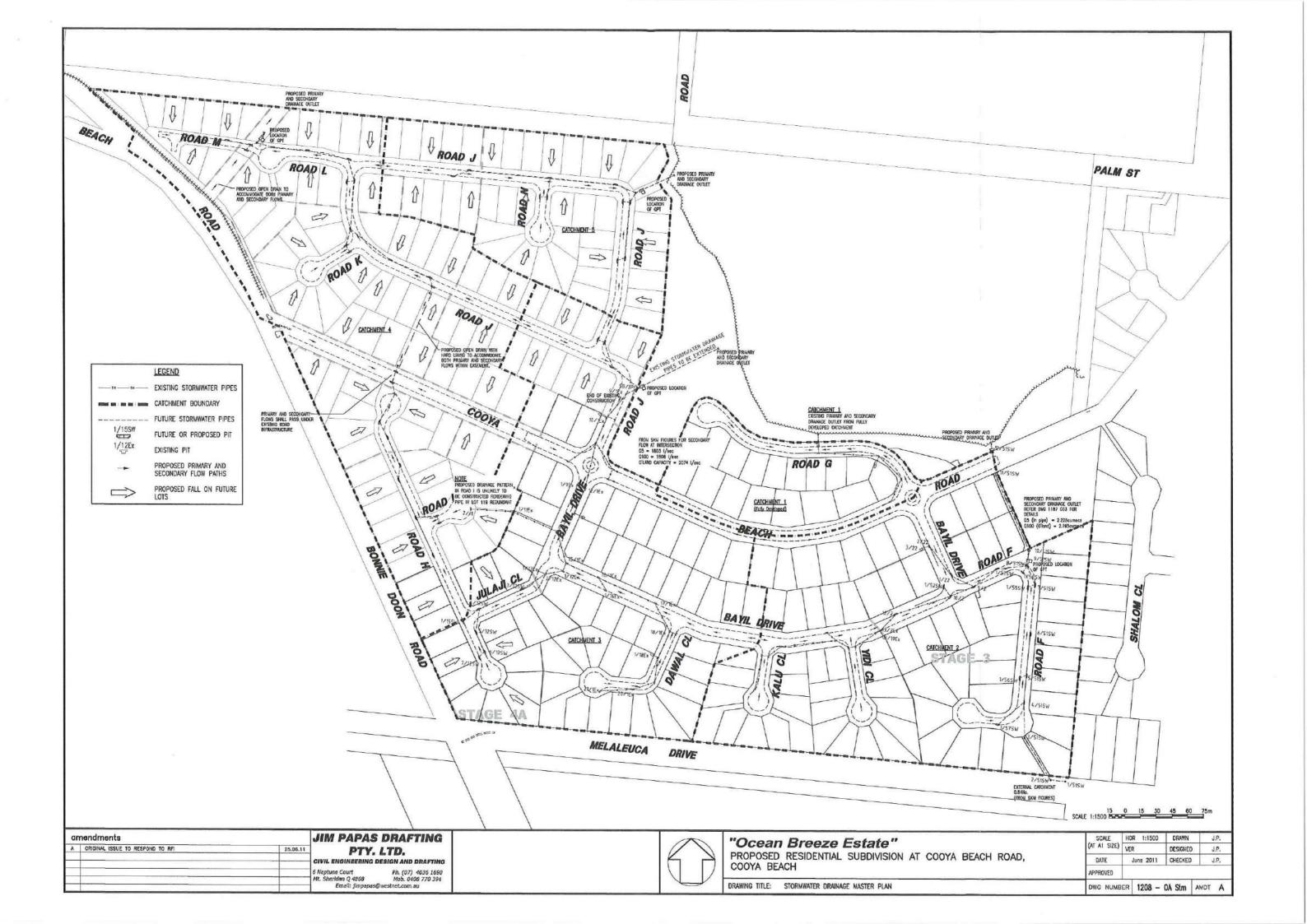
Appendix D: Dwg. 1208 OS Sewer



ACN 010 943 905 ABN 56 010 943 905

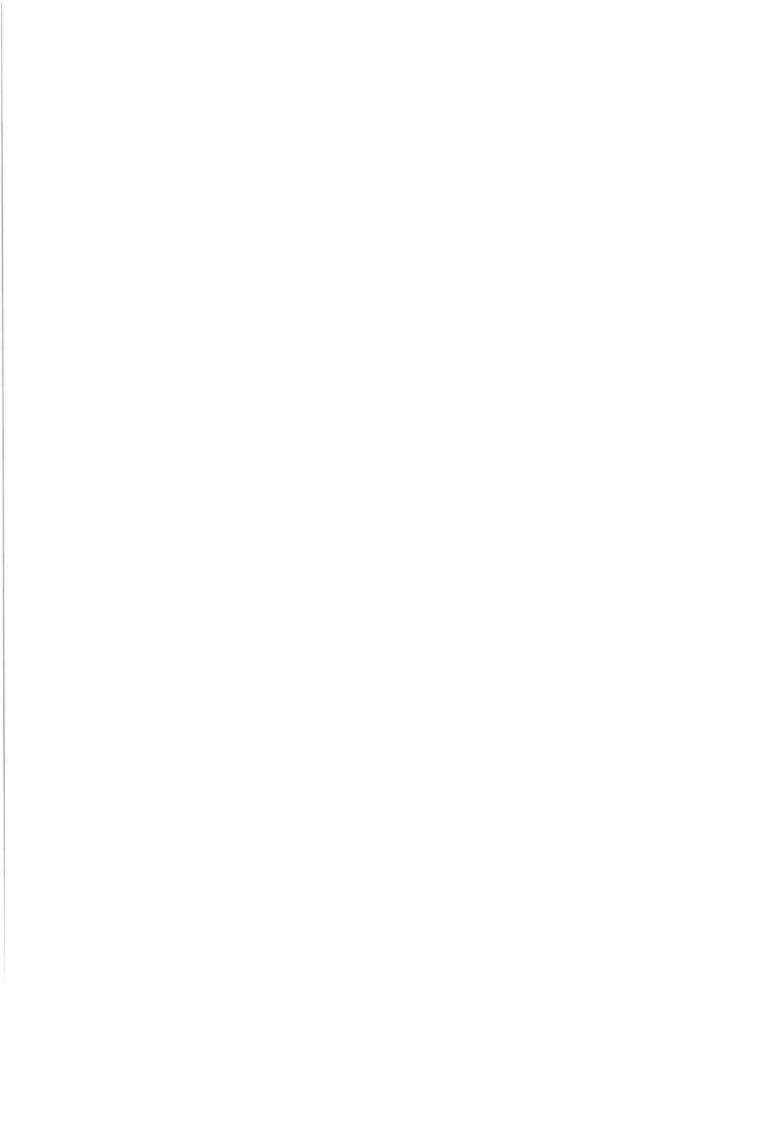
APPENDIX B STORMWATER DRAINAGE MASTER PLAN DWG. 1208 OA Stm

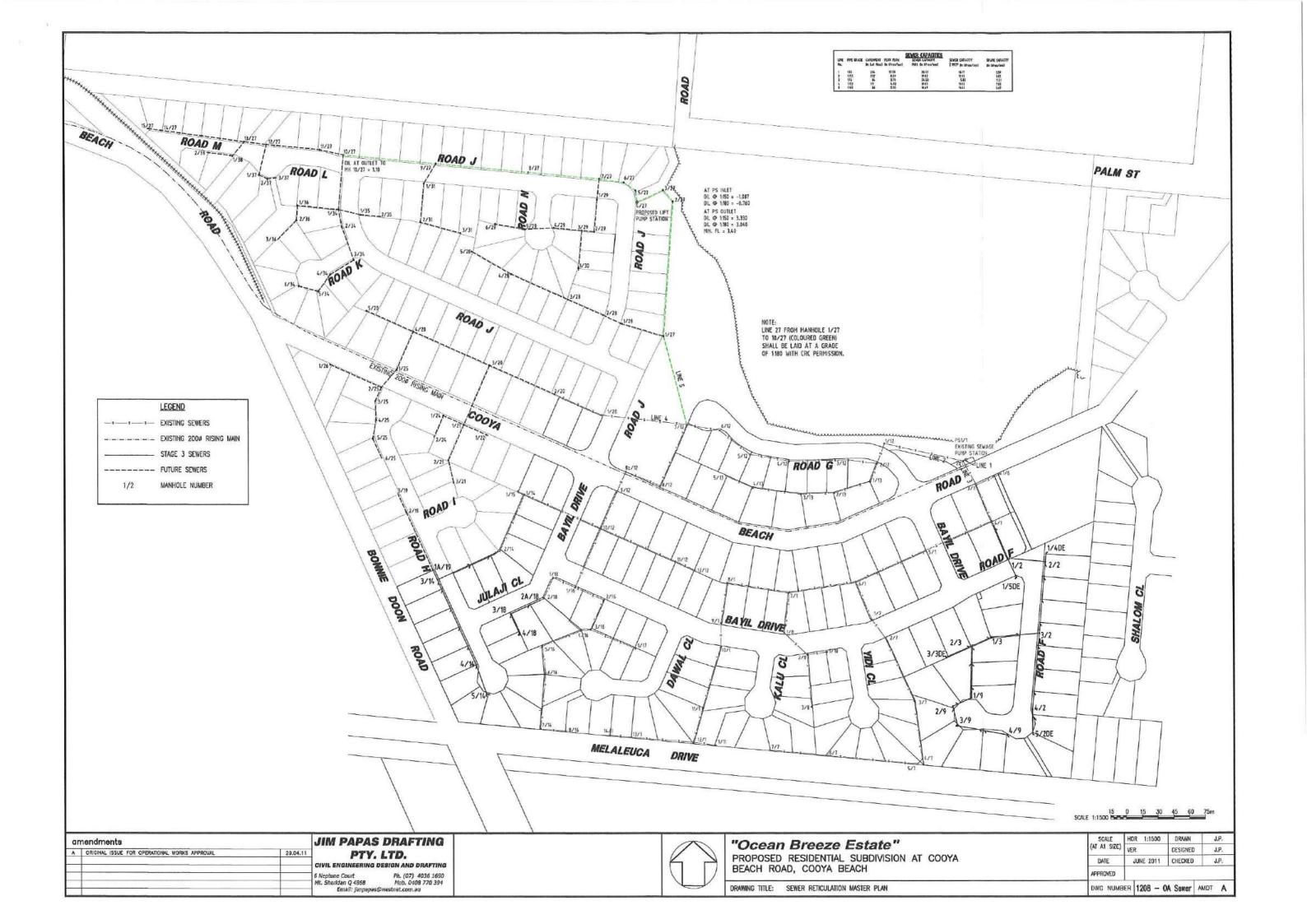




ACN 010 943 905 ABN 56 010 943 905

APPENDIX C WATER SUPPLY RETICULATION REPORT





PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

P.O. Box 413 Earlyille Q 4870

6 Neptune Court Mt. Sheridan Q 4868 Ph. (07) 4036 1690 FAX (07) 4036 4307 Mobile 0408 770 394

Email: jimpapas@westnet.com.au

WATER SUPPLY RETICULATION REPORT FOR OCEAN BREEZE ESTATE STAGE 4A

A

RESIDENTIAL SUBDIVISION

AT

COOYA BEACH ROAD

PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

1. INTRODUCTION

This report on the water supply reticulation for Ocean Breeze Estate, a residential subdivision at Cooya Beach, has been undertaken to show that a satisfactory level of water supply service is available to meet the interim and ultimate development requirements.

This report provides the necessary input model assumptions and results.

This report compliments another report prepared by SKM on the Cooya Beach water supply in March 2010.

2. MODELLING PARAMETERS

Model

The reticulation network was modelled using EPA Net Program Version 2. The model is based on a static analysis at peak hour.

This program analysed the reticulation network using Hazen-Williams head loss formula. Values of roughness coefficient 'c' used are in accordance with the FNQROC Development Manual requirements which are:

Diameter < 150 c=100 Diameter > 150 < 300 c=110

The three different scenarios were modeled. They are:

Scenario 1 - Fully developed domestic flow at peak hour

Scenario 2 - Fire fighting for and with appropriate peak hour demand imposed on the system

Scenario 3 - Fire fighting flow in Stage 4A

This modeling was divided into those separate scenarios to demonstrate that the existing trunk mains and water supply infrastructure can service the proposed development.

3. ASSUMPTIONS

- 1. No abnormal conditions affect the water supply
- 2. Construction of the development occurs in order of stage numbers
- 50 rider mains have not been modeled except between nodes 105 and 110 for compliance during stage construction

4. RESIDENTIAL DEMANDS

Demands

This model is based on the following demand:

- 1. Existing Cooya Beach demands
- 2. Proposed subdivision demands

The existing Cooya Beach demands are based on information provided by the former DCS to SKM This information is provided in Appendix C-1.

n at			
is			
in March			
in maron			
X.			
ed on a			
lues of			
ed on the			
nk mains			
liance			
lianoc			
- 01/24			
o SKM.			
	× .		

PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

The proposed subdivision demand is based on the current lot layout. These are summarised as follows:

Existing Cooya Beach demand external to the subject site:
(Includes an undeveloped lot comprising potentially 20 lots)

Existing demand from previous stages of the estate:

Ocean Breeze Stage 4A demand:

Demand in remaining stages of Ocean Breeze Estate:

280 lots

103 lots

167 lots

Total demand all lots at Cooya Beach:

568 lots

Surface elevations for the model nodes have been taken from the existing survey information provided by RPS. The survey data and existing lot layout is shown on Dwg 1280-OA Water. This drawing is attached as Appendix C-2.

The Cooya Beach demand has been modeled as a single point demand at Node 146. Refer the above mentioned drawing for details.

5. WATER SUPPLY REQUIREMENTS

The level of water supply service expected of the reticulated system is in accordance with the requirements of:

1. FNQROC Development Manual 'Water Reticulation Design Guidelines'

Department of Natural Resources and Mines 'Planning Guidelines for Water Supply and Sewerage'

Based on information from those documents the following data has been used in the model:

Average daily consumption (AD) = 500L/person

Single person dwelling

Lots < 900m²

2.8 persons per connection

Lots > 900m²

3.1 persons per connection

Peak day (PD) = 2.25 x AD

Peak hour = PD/12

Peak hour demand for lot < 900m² = 0.073L/sec

Peak hour demand for lot > 900m² = 0.081L/sec

These peak hour flows were allocated to the nodes and a static analysis used. The residential pressure at peak hour is required to be in the range of 22m to 60m head.

6. FIRE FIGHTING FLOW

The 'Planning Guidelines for Water Supply and Sewerage' provides that a system with a population of less than 2000 persons have the fire fighting flows imposed on ¾ of the peak hour demand. Cooya Beach has an approximate population of about 1700 persons which is well below the threshold noted above.

The water source for Cooya Beach is a reservoir reported by SKM to be 3.5MLcapacity. The required fire fighting flow is 15 L/sec for two hours and there is sufficient reservoir capacity for the fire fighting flow. We note that the external water reticulation works were constructed by an unrelated entity and our Clients have no responsibility whatsoever for any of this infrastructure. We offer no comment on any aspect of these works except to verify that they appear hydraulically adequate.

1			
vided			
ovided is			
10			
above			
above			
tion of			
ova			
oya noted			
auired			
htina			
and			
quired hting and ht on			

PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

The minimum permitted residential pressure during fire fighting flow is 12m. The maximum pressure network condition for modeling is based on reservoir level at 66% of top water level. Cairns Water advised SKM that all property services include a pressure-reducing device to cut pressure to approximately 50m per head. Therefore, separate and additional pressure reducing values are not required or any reticulation was within the development.

7. RESIDENTIAL PRESSURE

The maximum residual pressure available, assuming no demand, is about 66m.

Model results

The results of the modeling are shown in Appendix C-3.

Peak hour demand

The minimum required residential pressure at any mode during peak hour shall be greater than 22m. The residential pressure does not fall to less than this value at any stage.

SKM report noted that the reservoir servicing the site has the following characteristics:

1. TWL

69.61m

2. BWL

60.56m

3. Volume

3.5ML

Therefore:

95% of TWC = RL 69.16

66% of TWL = RL 66.53

The connection between Nodes 101 and 102 across Cooya Beach Road is provided to allow an alternative source of supply. This measure is good practice and enhances fire fighting flows but is not necessary during stage construction.

8. FIRE FIGHTING FLOW

The model was examined on a number of occasions to establish the most hydraulically disadvantaged hydrant. In the fully developed scenario the worst case was Node 124 in Stage 4A. The residual pressure at this node is 22.10m which is considerably greater than the required 12.0m.

At no node did the residual pressure all below 12.0m.

The model was also examined for performance during staged development and at no time did the residual pressure at any node fall below 12.0m.

9. CONCLUSIONS

For the analysis provided, it can be concluded that:

- The proposed water supply network within the subdivision as shown in Appendix B conforms
 with the requirements of both FNQROC Development Manual 'Water Reticulation Design
 Guidelines' and Department of Natural Resources and Mines 'Planning Guidelines for Water
 Supply and Sewerage'
- The proposed water supply network provides satisfactory fire fighting protection for the proposed development

ot			
ed			

PTY. LTD.

ACN 010 943 905 ABN 56 010 943 905

- 2. The proposed water supply network provides a satisfactory level of domestic water supply for all the proposed development
- 3. That the reticulation network within Cooya Beach has adequate capacity to meet future demands
- 4. No upgrading of existing water supply infrastructure is required as a result of the development

Recommend this report to Council for approval.

Attachments:

Appendix C-1:

Appendix C-2: Appendix C-3:

Existing Cooya Beach Demands. Water Supply Reticulation Master Plan

Model Results



ACN 010 943 905 ABN 56 010 943 905

APPENDIX C-1 EXISTING COOYA BEACH DEMANDS

	SIN	CLAIR KNIGHT	MERZ :+61	5
facsimile	REC'D	14 FEB 2005		
transmission	1 VYHO		AGMALO:	

TO: Waste Oum

COMPANY: 3Km

FAX NO: 4031 3967

- LOJECT No. OUR REF: FILE YOUR REF:

> DATE: 14 February 2005

DEPT: Engineering Services

PAGES: 4/ (Including this page)

FROM: Peter Cymbala

Enquiries to: Peter Cymbala
Douglas Shire Council, PO Box 357, Mossman Qtd 4873

Phone: Fax:

(07) 4099 9462 (07) 4098 2902

This faustinile is confidential and may be the subject of legal privilege. It is intended for the named addressee. If you are not the addressee, any use of this facsimile whatsoever or the information contained in it is prohibited. Please let us know immediately if you have received this communication in error so that we can arrange for it to be returned.

Mall:

Mall:

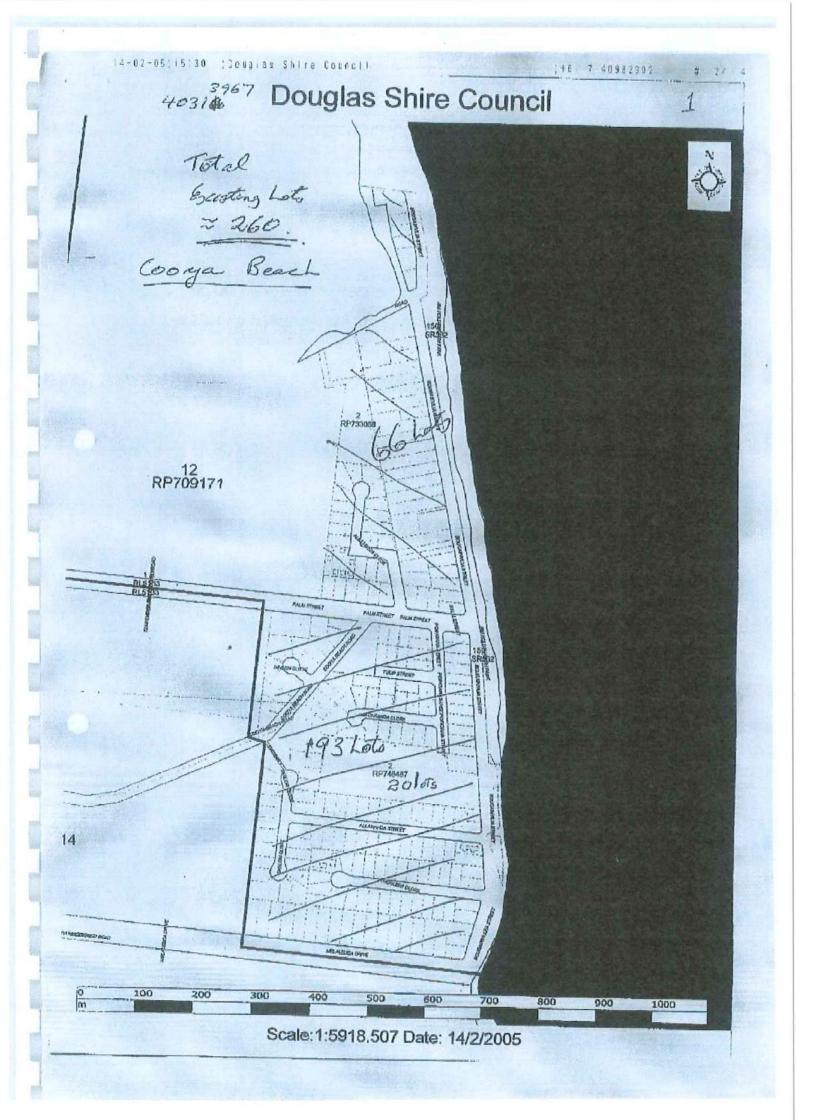
Massimile is confidential and may be the supportation facinities whatsoever or the information contained in it is produte can arrange for it to be returned.

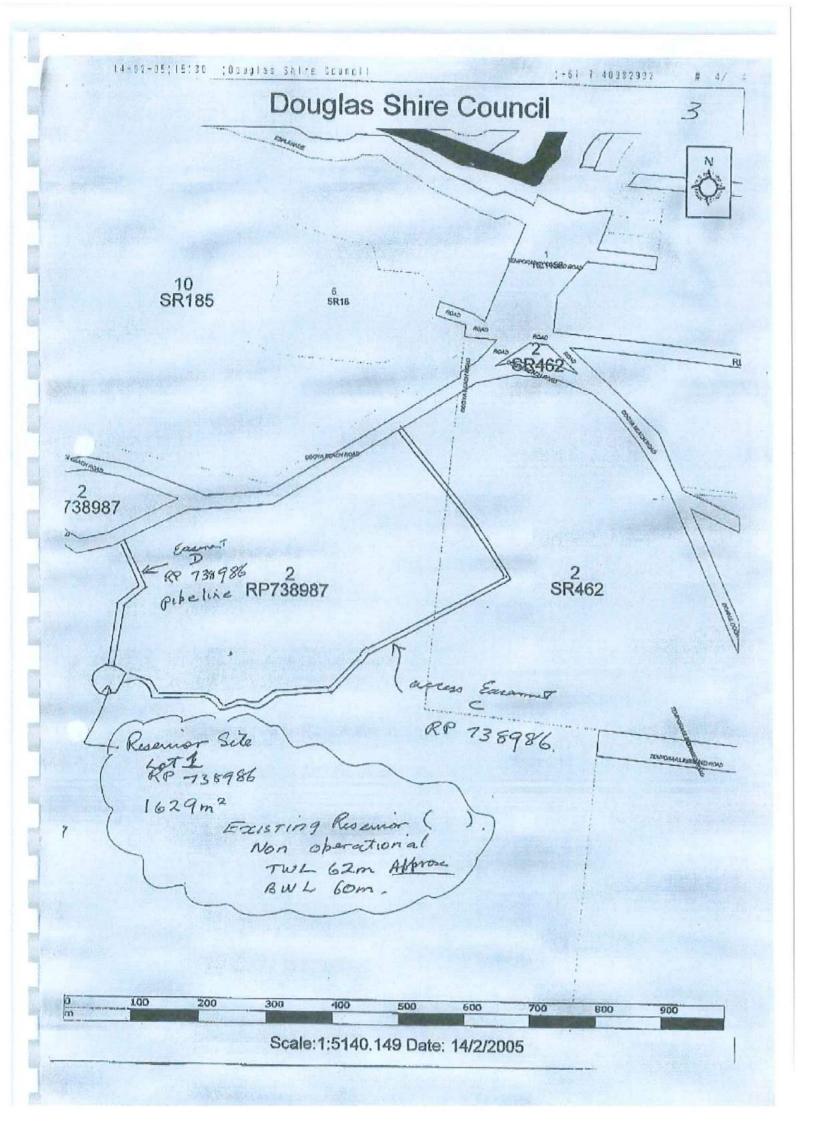
MESSAGE:

Co saya Beanh

Wacle

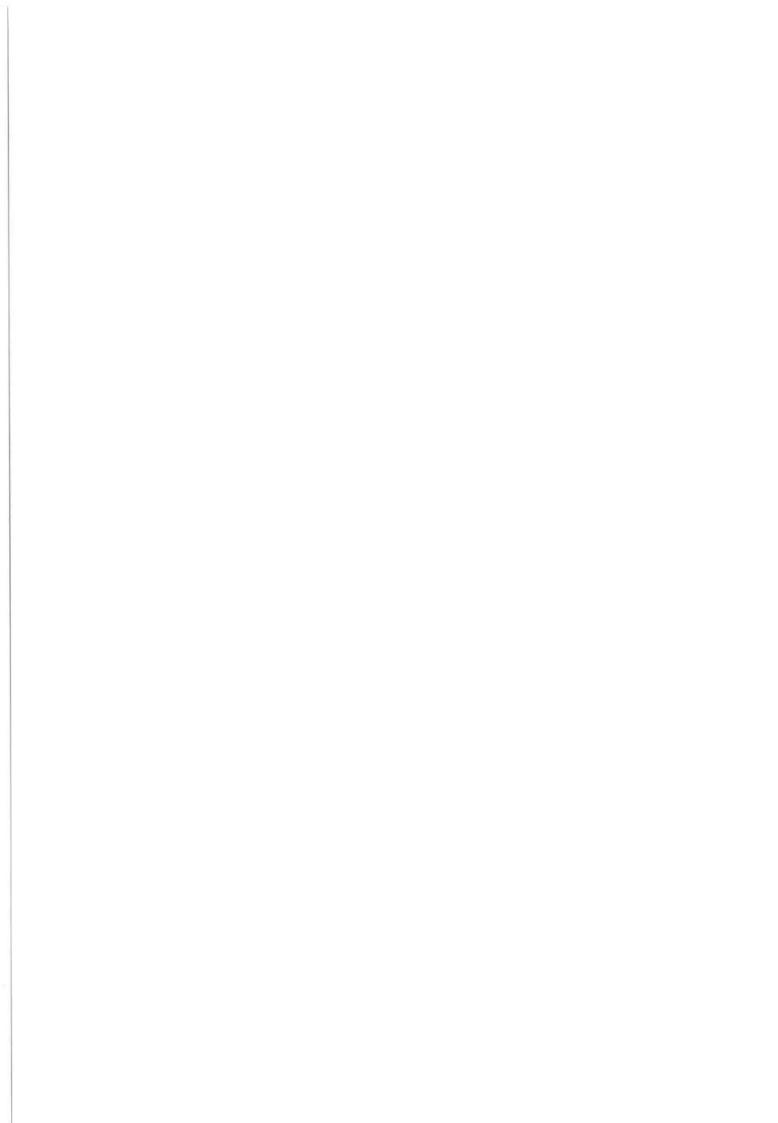
Jund attach shetcher of security services and Services an





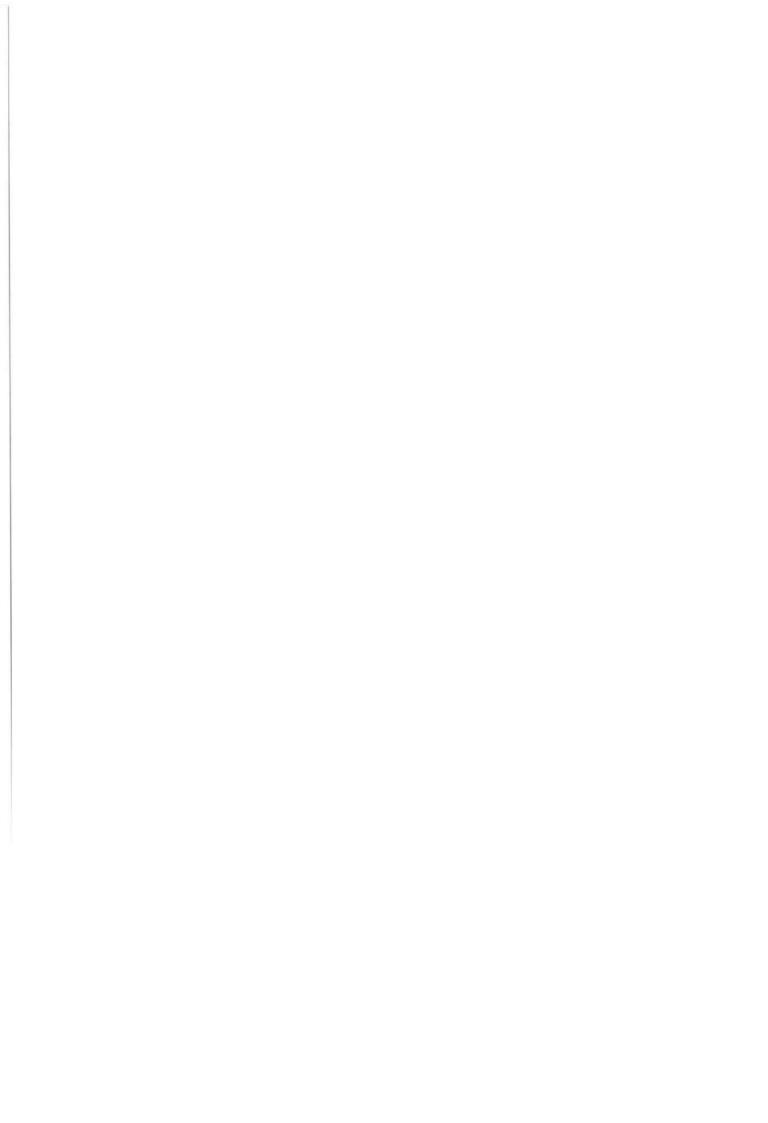
ACN 010 943 905 ABN 56 010 943 905

APPENDIX C-2 WATER RETICULATION MASTER PLAN



ACN 010 943 905 ABN 56 010 943 905

APPENDIX C-3
MODEL RESULTS



Input File: 1208 Domestic Peak Hour Flows.net

Link - Node Table:

	: Table.			
Link ID	Start Node	End Node	Length m	Diameter mm
2	101	102	30	104.3
3	102	110	183	104.3
4	101	118	248	202.2
2 3 4 5 6 7 8	110	111	23	104.3
6	111	103	11 77	104.3
7	111	108	77	104.3
8	111	112	165	104.3
9	112	-LLT		104.3
10	112	14	22 11	104.3
11	112	104	_ 11	104.3
12	14	107	216	104.3
13	107	106	24	104.3
14	106	105	36	104.3
15	107	108	233	104.3
16	108	109	83	104.3
17	105	115	60	104.3
18	115	116	29	104.3
19	116	117	244	104.3
20	116	120	15	104.3
21	117	118	15	104.3
22 23	118	119	56 188 154	202.2
23	119	120	188	202.2
24	119	126	134	104.3
25	120	121 142	95 170	104.3 202.2
26	120 121	122	42	104.3
27	121	130	150	104.3
28 29	122	129	61	104.3
30	129	123	22	104.3
31	123	124	68	104.3
32	126	128	20	104.3
33	128	125	10	104.3
34	128	127	57	104.3
35	128	129	78	104.3
36	130	131	175	104.3
37	130	132	87	104.3
38	132	133	121	104.3
30	132	133	121	104.3

Page 2 Link - Node Table: (continued)

Link ID	Start Node	End Node	Length m	Diameter mm
39	132	134	79	104.3
40	134	135	145	104.3
41	134	136	25	104.3
42	136	137	65	104.3
43	137	147	80	104.3
44	137	138	81	104.3

		1208 Domestic Peak Hou	r Flows.rpt	
45	138	139	13	104.3
46	138	145	85	104.3
47	139	140	86	104.3
48	139	143	15	104.3
49	140	141	173	104.3
50	141	115	90	104.3
51	142	143	167	202.2
52	143	144	241	104.3
53	143	145	76	202.2
54	145	146	142	202.2
55	147	148	216	104.3
1	50	101	1075	202.2
56	109	110	157	48.4
57	105	108	288	48.4

Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality	
101 102 103 104 105 106 107 108 109 110 111 112 114 14 115 116 117 118 119 120	0.00 0.66 0.66 0.66 0.80 0.73 0.44 0.80 0.58 0.37 0.29 0.44 0.51 0.07 0.49 0.41 0.16 0.54 0.39	56.48 48.66 48.70 48.72 49.74 49.37 49.18 48.76 48.73 48.72 48.72 48.72 48.75 50.60 51.34 53.55 53.06 51.45	52.98 45.26 44.90 45.32 45.64 45.27 44.78 44.76 41.63 45.29 44.90 45.32 43.52 45.35 45.70 46.80 46.75 47.76	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	
121	0.15	50.53	43.63	0.00	

Page 3 Node Results: (continued)

Node ID	Demand LPS	Head m	Pressure m	Quality	
122	0.15	50.46		0.00	
123	0.27	50.35	44.05	0.00	
124	0.73	50.34	43.64	0.00	
125	0.51	50.32		0.00	
126	0.29	50.32		0.00	
127	0.29	50.32		0.00	
128	0.07	50.32	44.52	0.00	
129	0.07	50.36	44.16	0.00	
130	0.51	50.01		0.00	
131	0.51	49.99	42.99	0.00	
132	0.37	49.85	42.85	0.00	
133	0.80	49.82	42.72	0.00	
134	0.22	49.81		0.00	
135	0.22	49.76	43.76	0.00	
				1.급하루어급하급하	
136	0.49	49.81	45.21	0.00	
137	0.08	49.81	45.91	0.00	
138	0.22	49.97	44.77	0.00	
139	0.16	50.05	44.75	0.00	
140	0.32	50.15	43.35	0.00	

	1208 D	omestic Pea	k Hour Flo	ws.rpt
141	0.41	50.41	44.51	0.00
142	0.56	50.75	43.65	0.00
143	0.31	50.09	44.69	0.00
144	0.58	50.06	44.86	0.00
145	0.69	49.87	46.47	0.00
146	20.44	49.43	46.43	0.00
147	0.81	49.71	46.31	0.00
148	1.22	49.60	44.50	0.00
50	-41.62	69.16	0.00	0.00 Reservoir

Link Results:

Link	Flow	VelocityUnit	Headloss	Status	
ID	LPS	m/s	m/km	Jeacus	
2	0.00	0.00	0.00	Closed	
3	-0.66	0.08	0.16	Open	
4	41.62	1.30	11.80	Open	
5	-1.12	0.13	0.44	Open	
6	0.66	0.08	0.16	Open	
7	-1.52	0.18	0.77	Open	
8	-0.64	0.07	0.15	Open	
9	0.44	0.05	0.08	Open	
10	-2.03	0.24	1.31	Open	
11	0.66	0.08	0.16	Open	
12	-2.54	0.30	1.99	Open	
13	-5.40	0.63	8.06	Open	
14	-6.13	0.72	10.19	Open	

Page 4 Link Results: (continued)

Link ID	Flow LPS	VelocityUnit m/s	Headloss m/km	Status	
15	2.42	0.28	1.82	Open	
16	0.92	0.11	0.30	Open	
17	-7.38	0.86	14.37	Open	
18	-10.06	1.18	25.53	Open	
19	-5.54	0.65	8.44	Open	
20	-5.02	0.59	7.03	0pen	
21	-5.95	0.70	9.64	open	
22	35.51	1.11	8.79	Open	
23	34.97	1.09	8.55	Open	
24	0.00	0.00	0.00	Closed	
25	5.96	0.70	9.69	Open	
26	23.60	0.74	4.13 1.77	Open	
27 28	2.38	0.28		Open	
29	3.43 2.23	0.40 0.26	3.48 1.57	Open Open	
30	1.00	0.12	0.35	Open	
31	0.73	0.09	0.20	Open Open	
32	-0.29	0.03	0.04	Open	
33	0.51	0.06	0.10	Open	
34	0.29	0.03	0.04	Open	
35	-1.16	0.14	0.47	Open	
36	0.51	0.06	0.10	Open	
37	2.41	0.28	1.81	Open	
38	0.80	0.09	0.23	Open	
39	1.24	0.15	0.53	Open	
40	0.95	0.11	0.32	Open	
41	0.07	0.01	0.00	Open	
42	-0.42	0.05	0.07	Open	
43	2.03	0.24	1.32	0pen	
44	-2.53	0.30	1.97	0pen	
45	-4.63	0.54	6.07	Open	
46	1.89	0.22	1.15	Open	

	1208	Domestic Peal	Hour Flo	ws.rpt
47	-1.88	0.22	1.15	Open
48	-2.91	0.34	2.56	Open
49	-2.20	0.26	1.53	Open
50	-2.61	0.31	2.10	Open
51	23.04	0.72	3.95	open
52	0.58	0.07	0.13	open
53	19.24	0.60	2.83	Open
54	20.44	0.64	3.16	Open
55	1.22	0.14	0.51	open
1	41.62	1.30	11.80	open
56	0.12	0.06	0.28	Open
57	0.45	0.25	3.42	Open

1208 Fire Fighting Flow at Peak Hour Flows.rpt Page 1 25/06/2011 1:47:10 PM EPANET

Input File: 1208 Fire Fighting Flow at Peak Hour Flows.net

Link - Node Table:

Link - No				
Link ID	Start Node	End Node	Length m	
2	101	102	30	104.3
3	102	110	183	104.3
4	101	118	248	202.2
5 6 7	110	111	23	104.3
6	111	103	11	104.3
/	111	108	77	104.3
8	111	112	165	104.3
10	112 112	114	67	104.3
10	112 112	14	22	104.3
11 12	112 14	104 107	11 216	104.3
13	107	106	24	104.3 104.3
14	106	105	36	104.3
15	107	103	233	104.3
16	108	109	83	104.3
17	105	115	60	104.3
18	115	116	29	104.3
19	116	117	244	104.3
20	116	120	15	104.3
21	117	118	15	104.3
22	118	119	56	202.2
23	119	120	188	202.2
24	119	126	154	104.3
25	120	121	95 170	104.3
26	120	142	170	202.2
27	121	122	42	104.3
28	121	130	150	104.3
29	122	129	61	104.3
30	129	123	22	104.3
31	123	124	68	104.3
32	126	128	20	104.3
33	128	125	10	104.3
34	128	127	57	104.3
35	128	129	78	104.3
36	130	131	175	104.3
37	130	132	87	104.3
38	132	133	121	104.3

Page 2 Link - Node Table: (continued)

Link	Start	End	Length	Diameter
ID	Node	Node	m	mm
39	132	134	79	104.3
40	134	135	145	104.3
41	134	136	25	104.3
42	136	137	65	104.3
43	137	147	80	104.3
44	137	138	81	104.3

	1208	Fire Fighting	Flow at	Peak	Hour	Flows	.rpt
45	138	139				13	104.3
46	138	145				85	104.3
47	139	140				86	104.3
48	139	143				15	104.3
49	140	141				173	104.3
50	141	115				90	104.3
51	142	143				167	202.2
52	143	144				241	104.3
53	143	145				76	202.2
54	145	146				142	202.2
53 54 55	147	148				216	104.3
1	50	101			1	L075	202.2
56 57	109	110				157	48.4
57	105	108				288	48 4

Node Results:

Noue Results.					
Node	Demand		Pressure	Quality	
ID	LPS	m	m		
101	0.00	53.19	49.69	0.00	
102	0.44	46.36	42.96	0.00	
103	0.44	46.38	42.58	0.00	
104	0.44	46.39	42.99	0.00	
105	0.53	46.87	42.77	0.00	
106	0.49	46.70	42.60	0.00	
107	0.29	46.61		0.00	
108	0.29	46.41	42.41	0.00	
109	0.53	46.40	39.30	0.00	
110	0.39	46.37	42.97	0.00	
111	0.25	46.38	42.58	0.00	
112	0.19	46.39	42.99	0.00	
114	0.29	46.39		0.00	
14	0.34	46.41	43.01	0.00	
115	0.05	47.28	42.38	0.00	
116	0.33	47.82	42.22	0.00	
117	0.27	49.97	43.37	0.00	
118	0.11	50.11	43.31	0.00	
119	0.36	49.59	44.29	0.00	
120	0.26	47.86		0.00	
121	0.10	46.22	39.32	0.00	

Page 3 Node Results: (continued)

Node ID	Demand LPS		Pressure m	Quality	
122	0.10	46.19	39.29	0.00	
123			39.84		
124			39.43		
125			40.43		
126			40.43		
127	0.19		39.73	0.00	
128	0.05		40.33		
129	0.05	46.14		0.00	
130	0.34		37.49		
131	0.34	44.54		0.00	
132		43.75			
133	0.53	43.74		0.00	
134		43.20			
135	0.63	43.18	37.18	0.00	
136	0.33		38.48	0.00	
137			38.89		
138	0.15	45.90		0.00	
139	0.11		40.89		
140	0.21		39.62		
			ige 2	850005250	

	1208 Fire Figh	iting Flow	at Peak Hou	ır Flows.rpt
141	0.27	46.96	41.06	0.00
142	0.37	47.09	39.99	0.00
143	0.21	46.35	40.95	0.00
144	0.39	46.34	41.14	0.00
145	0.46	46.17	42.77	0.00
146	13.63	45.96	42.96	0.00
147	0.54	37.77	34.37	0.00
148	15.82	25.02	19.92	0.00
50	-42 77	66.53	0.00	0.00 Reservoir

Link Results:

		Volocity/Init	dloss	Ctatus	
Link ID	Flow LPS	VelocityUnit m/s	m/km	Status	
2	0.00	0.00	0.00	Closed	
3	-0.44	0.05	0.08	Open	
4	42.77	1.33	12.41	Open	
5	-0.75	0.09	0.21	Open	
6	0.44	0.05	0.08	Open	
7	-1.01	0.12	0.36	Open	
8	-0.43	0.05	0.07	Open	
9	0.29	0.03	0.04	Open	
10	-1.35	0.16	0.62	Open	
11	0.44	0.05	0.08	Open	
12	-1.69	0.20	0.94	Open	
13	-3.60	0.42	3.81	Open	
14	-4.09	0.48	4.81	Open	

Page 4 Link Results: (continued)

15	Link ID	LPS	VelocityUnit m/s	Headloss m/km	Status	
17 18 18 18 18 18 18 18 18 18 18 18 18 18	15	1.62	0.19	0.86	Open	
18 -8.46 0.99 18.53 Open 19 -5.67 0.66 8.81 Open 20 -3.12 0.37 2.93 Open 21 -5.94 0.70 9.62 Open 22 36.72 1.14 9.36 Open 23 36.36 1.13 9.19 Open 24 0.00 0.00 0.00 Closed 25 8.14 0.95 17.23 Open 26 24.84 0.77 4.54 Open 27 1.59 0.19 0.83 Open 28 6.45 0.75 11.20 Open 29 1.49 0.17 0.74 Open 30 0.67 0.08 0.17 Open 31 0.49 0.06 0.09 Open 32 -0.19 0.02 0.02 Open 34 0.19 0.02 0.02 Open 35 -0.77 0.09 0.22 Open 36		0.61				
19			0.58	6.79	Open	
20			0.99		Open	
21			0.66	8.81	Open	
22 36.72 1.14 9.36 Open 23 36.36 1.13 9.19 Open 24 0.00 0.00 Closed 25 8.14 0.95 17.23 Open 26 24.84 0.77 4.54 Open 27 1.59 0.19 0.83 Open 28 6.45 0.75 11.20 Open 29 1.49 0.17 0.74 Open 30 0.67 0.08 0.17 Open 31 0.49 0.06 0.09 Open 32 -0.19 0.02 0.02 Open 34 0.19 0.02 0.02 Open 34 0.19 0.02 0.02 Open 35 -0.77 0.09 0.22 Open 36 0.34 0.04 0.05 Open 37 5.77 0.68 9.11 Open 39 4.99 0.58 6.96 Open 40 0.63 <td< td=""><td>20</td><td></td><td>0.37</td><td></td><td></td><td></td></td<>	20		0.37			
23 36.36 1.13 9.19 Open 24 0.00 0.00 Closed 25 8.14 0.95 17.23 Open 26 24.84 0.77 4.54 Open 27 1.59 0.19 0.83 Open 28 6.45 0.75 11.20 Open 29 1.49 0.17 0.74 Open 30 0.67 0.08 0.17 Open 31 0.49 0.06 0.09 Open 32 -0.19 0.02 0.02 Open 34 0.19 0.02 0.02 Open 34 0.19 0.02 0.02 Open 36 0.34 0.04 0.05 Open 37 5.77 0.68 9.11 Open 39 4.99 0.58 6.96 Open 40 0.63 0.07 0.15 Open 41 4.21 0.49 5.08 Open 42 3.88 0	21					
24 0.00 0.00 0.00 closed 25 8.14 0.95 17.23 open 26 24.84 0.77 4.54 open 27 1.59 0.19 0.83 open 28 6.45 0.75 11.20 open 29 1.49 0.17 0.74 open 30 0.67 0.08 0.17 open 31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 40 0.63 0.07 0.15 open 40 0.63 0.07 0.15 open 41 4	22					
25 8.14 0.95 17.23 open 26 24.84 0.77 4.54 open 27 1.59 0.19 0.83 open 28 6.45 0.75 11.20 open 29 1.49 0.17 0.74 open 30 0.67 0.08 0.17 open 31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -	23					
26 24.84 0.77 4.54 Open 27 1.59 0.19 0.83 Open 28 6.45 0.75 11.20 Open 29 1.49 0.17 0.74 Open 30 0.67 0.08 0.17 Open 31 0.49 0.06 0.09 Open 32 -0.19 0.02 0.02 Open 34 0.04 0.05 Open 35 -0.77 0.09 0.22 Open 36 0.34 0.04 0.05 Open 37 5.77 0.68 9.11 Open 38 0.53 0.06 0.11 Open 40 0.63 0.07 0.15 Open 41 4.21 0.49 5.08 Open 42 3.88 0.45 4.37 Open 43 16.36 1.91 62.80 Open 45 -9.35 1.09 22.30 Open			0.00	0.00		
1.59			0.95			
28 6.45 0.75 11.20 open 29 1.49 0.17 0.74 open 30 0.67 0.08 0.17 open 31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 40 0.63 0.07 0.15 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45	26					
29 1.49 0.17 0.74 open 30 0.67 0.08 0.17 open 31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 40 0.63 0.07 0.15 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open			0.19	0.83		
30 0.67 0.08 0.17 open 31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 40 0.63 0.07 0.15 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open				11.20		
31 0.49 0.06 0.09 open 32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open	29			0.74		
32 -0.19 0.02 0.02 open 33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open						
33 0.34 0.04 0.05 open 34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open						
34 0.19 0.02 0.02 open 35 -0.77 0.09 0.22 open 36 0.34 0.04 0.05 open 37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open	32					
35	33					
36 0.34 0.04 0.05 Open 37 5.77 0.68 9.11 Open 38 0.53 0.06 0.11 Open 39 4.99 0.58 6.96 Open 40 0.63 0.07 0.15 Open 41 4.21 0.49 5.08 Open 42 3.88 0.45 4.37 Open 43 16.36 1.91 62.80 Open 44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open	34					
37 5.77 0.68 9.11 open 38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open	35					
38 0.53 0.06 0.11 open 39 4.99 0.58 6.96 open 40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open	36					
39 4.99 0.58 6.96 Open 40 0.63 0.07 0.15 Open 41 4.21 0.49 5.08 Open 42 3.88 0.45 4.37 Open 43 16.36 1.91 62.80 Open 44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open						
40 0.63 0.07 0.15 open 41 4.21 0.49 5.08 open 42 3.88 0.45 4.37 open 43 16.36 1.91 62.80 open 44 -12.53 1.47 38.33 open 45 -9.35 1.09 22.30 open						
41 4.21 0.49 5.08 Open 42 3.88 0.45 4.37 Open 43 16.36 1.91 62.80 Open 44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open	39					
42 3.88 0.45 4.37 Open 43 16.36 1.91 62.80 Open 44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open						
43 16.36 1.91 62.80 Open 44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open						
44 -12.53 1.47 38.33 Open 45 -9.35 1.09 22.30 Open		3.88	0.45		0.700 7 0.000,0000	
45 -9.35 1.09 22.30 Open		16.36	1.91	62.80		
		-12.53	1.4/	38.33		
46 -3.33 0.39 3.29 Open						
	46	-3.33	0.39	3.29	open	

	1208 Fire	Fighting	Flow at	Peak H	our Flo	ws.rpt
47	-3.		.35	2.73	Ope	
48	-6.	45 0	.76	11.21	Ope	n
49	-3.	22 0	.38	3.10	Ope	en
50	-3.	50 0	.41	3.60	Ope	n
51	24.	47 0	.76	4.41	Ope	n
52	0.	39 0	.05	0.06	Ope	n
53	17.	42 0	. 54	2.35	Ope	en
54	13.	63 0	.42	1.49	Ope	en
55	15.	82 1	.85	59.01	Ope	n
1	42.	77 1	.33	12.41	Ope	en
56	0.	08 0	.04	0.13	Ope	en
57	0.	30 0	.16	1.62	Ope	n

Input File: 1208 Fire Fighting Flow at Peak Hour Flows for Stage 4.net

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm	_
2	101	102	30	104.3	-
2 3 4 5 6 7 8 9	102	110	183	104.3	
4	101	118	248	202.2	
5	110	111	23	104.3	
6	111	103	11	104.3	
7	111	108	77	104.3	
8	111	112	165	104.3	
9	112	114	67	104.3	
10	112	14	22 11	104.3	
11	112 14	104	216	104.3	
12 13	107	107 106	24	104.3 104.3 104.3 104.3	
14	106	105	36	104.3	
15	107	108	233	104.3	
16	108	109	83	104.3	
17	105	115	60	104.3	
18	115	116	29	104.3	
19	116	117	244	104.3	
20	116	120	15	104.3	
21	117	118	15	104.3	
22	118	119	15 56	202.2	
23	119	120	188	202.2	
24	119	126	188 154	104.3	
25	120	121	95	104.3	
25 26	120	142	95 170	202.2	
27	121	122	42	104.3	
28	121	130	150	104.3	
29	122	129	61	104.3	
30	129	123	22	104.3	
31	123	124	68	104.3	
32	126	128	20	104.3	
33	128	125	10	104.3	
34	128	127	57	104.3	
35	128	129	78	104.3	
36	130	131	175	104.3	
37	130	132	87	104.3	
38	132	133	121	104.3	

Page 2 Link - Node Table: (continued)

Link ID	Start Node	End Node	Length m	Diameter mm
39	132	134	79	104.3
40	134	135	145	104.3
41	134	136	25	104.3
42	136	137	65	104.3
43	137	147	80	104.3
44	137	138	81	104.3

	1208	Fire	Fighting	Flow at	Peak Hour	Flows	for	Stage 4.rpt
45		138	9 9	139			13	104.3
46		138		145			85	104.3
47		139		140			86	104.3
48		139		143			15	104.3
49		140		141			173	104.3
50		141		115			90	104.3
51		142		143			167	202.2
52		143		144			241	104.3
53		143		145			76	202.2
54		145		146			142	202.2
55		147		148			216	104.3
1		50		101			1075	202.2
56		109		110			157	48.4
57		105		108			288	48.4

Node Results:

Node	Demand	Head	Pressure	Quality	
ID	LPS	m	m		
101	0.00	53.19	49.69	0.00	
102	0.44-26	49181.00	-2649184.00	0.00	
103	0.44-26	49181.00	-2649185.00	0.00	
104	0.44-26	49181.00	-2649185.00	0.00	
105			-2649185.00		
106	0.49-26	49181.00	-2649185.00	0.00	
107	0.29-26	49181.00	-2649186.00	0.00	
108	0.29-26	49181.00	-2649185.00	0.00	
109	0.53-26	49181.00	-2649188.00	0.00	
110	0.39-26	49181.00	-2649184.00	0.00	
111			-2649185.00	250.505.50	
112	0.19-26	49181.00	-2649185.00	0.00	
114	0.29-26	49181.00	-2649186.00	0.00	
14	0.34-26		-2649185.00		
115	0.05	48.27		0.00	
116			42.84	0.00	
117			43.71		
118		50.43		0.00	
119		49.96		0.00	
120		48.44		0.00	
121	0.10	40.12	33.22	0.00	

Page 3 Node Results: (continued)

Node	Demand	Head	Pressure	Quality	
ID	LPS	m	m	•	
122	0.10	37.53	30.63	0.00	
123	0.18	32.53	26.23	0.00	
124	15.49	28.67	21.97	0.00	
125	0.34-4	16368.50-	416374.20	0.00	
126	0.19-4	16368.50-	416374.20	0.00	
127			416374.80	0.00	
128			416374.30	0.00	
129	0.05			0.00	
130	0.34			0.00	
131	0.34			0.00	
132	0.25		32.46	0.00	
133	0.53		32.35		
134	0.15			0.00	
135			33.36	0.00	
136	0.33	39.37		0.00	
137			757396.40	0.00	
138		47.87			
139		47.89		0.00	
140	0.21	47.96	41.16	0.00	

	1208	Fire	Fiahtina	Flow at Peak	Hour Flows	for Stage 4.rpt
141			0.27	48.15	42.25	0.00
142			0.37	48.16	41.06	0.00
143			0.21	47.90	42.50	0.00
144			0.39	47.88	42.68	0.00
145			0.46	47.80	44.40	0.00
146			13.63	47.59	44.59	0.00
147			0.54 - 7	757392.60-757	395.90	0.00
148			0.81-7	757392.60-757	397.80	0.00
50			-42 77	66.53	0.00	0.00 Reservoir

Link Results:

LTIK KCSUTCS.				
Link ID	Flow LPS	VelocityUnit m/s	Headloss m/km	Status
2	0.00	0.00	0.00	Closed
4	2.02 40.31	0.24 1.26	$0.00 \\ 11.12$	Open Open
5 6	1.53 0.44	0.18 0.05	13.25	Open Open
7 8	0.23 0.61	0.03	0.00	Open Open
9	0.29	0.03	0.00	Open
10 11	-0.32 0.44	0.04 0.05	$0.00 \\ 0.00$	Open Open
12 13	-0.66 -1.33	$0.08 \\ 0.16$	$0.00 \\ 12.70$	Open Open
14	-1.82	0.21	0.00	Open

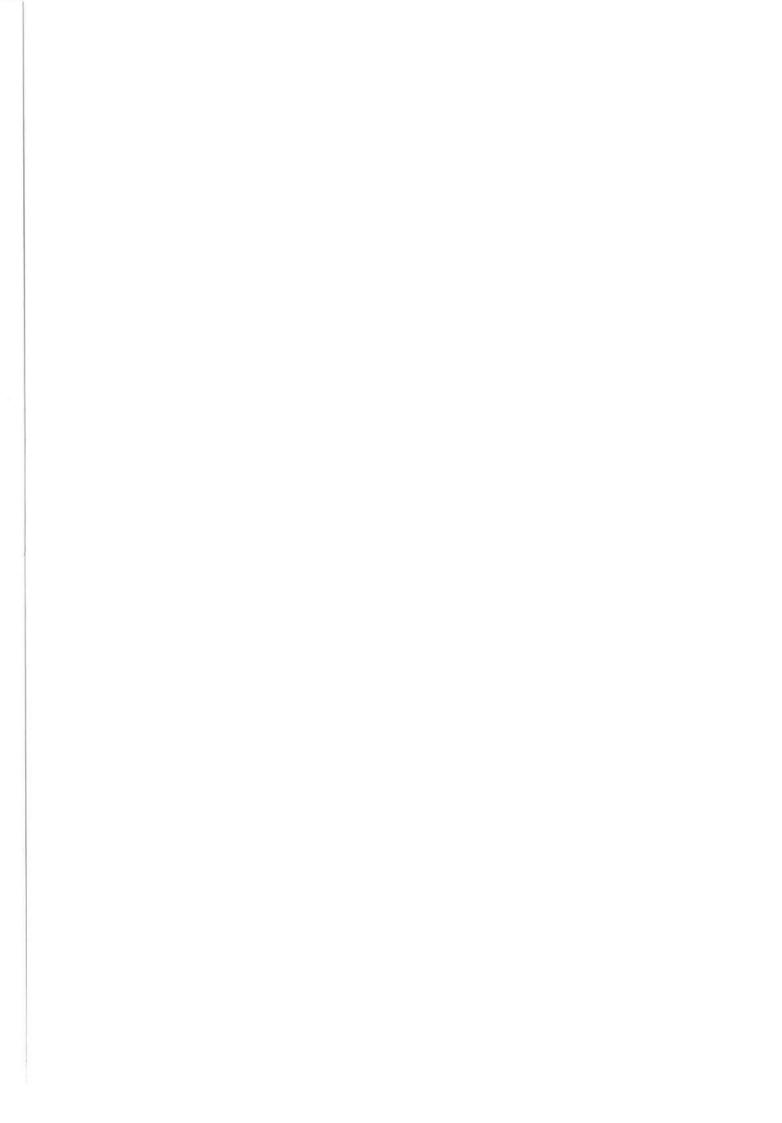
Page 4 Link Results: (continued)

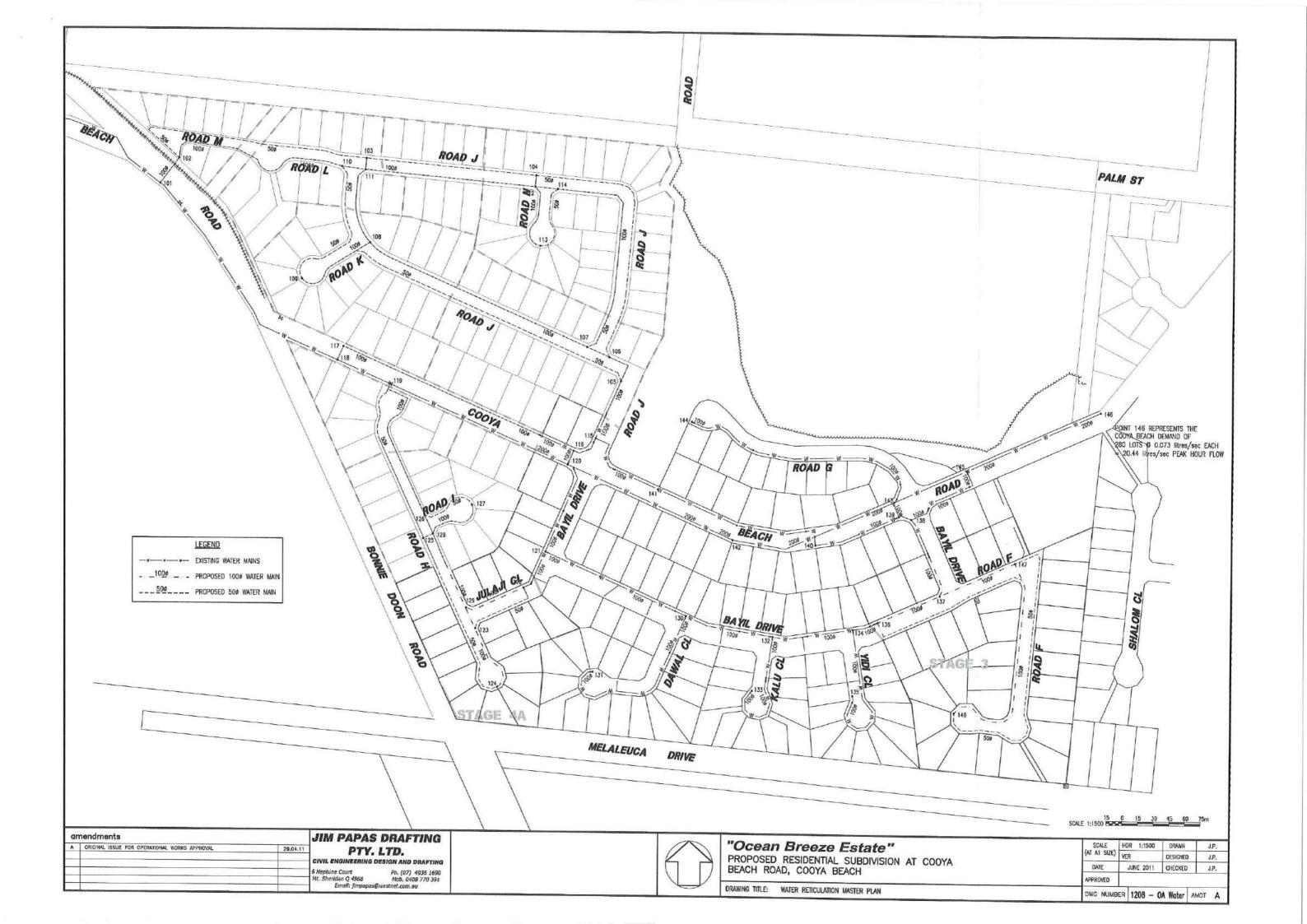
Link Results:	(continued)				
Link ID	Flow LPS	VelocityUnit m/s	Headloss m/km	Status	
1D 	0.39 0.43 0.00 -4.58 -5.25 0.33 -5.52 34.68 33.93 0.00 19.58 14.43 16.21 3.27 16.11 15.67 15.49 0.19 0.34 0.19 0.00 0.34 2.59 0.53 1.81	m/s 0.05 0.05 0.00 0.54 0.61 0.04 0.65 1.08 1.06 0.00 2.29 0.45 1.90 0.38 1.89 1.83 1.81 0.02 0.04 0.02 0.04 0.02 0.04 0.02 0.04 0.30 0.06 0.21	m/km 0.00 0.00 0.00 5.95 7.64 0.05 8.40 8.42 8.08 0.00 87.58 1.66 61.72 3.19 61.01 58.01 56.78 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Open Open Open Open Open Open Open Open	
40 41 42 43 44	0.63 1.03 0.00 1.35 0.00	0.07 0.12 0.00 0.16 0.00	0.15 0.38 0.00 0.95 0.00	Open Open Closed Open Closed	
45 46	-2.41 1.56	0.28 0.18	1.81 0.81	Open Open	

	1208	Fire	Fighting	Flow at Peak	Hour Flows	for Stage 4.rpt
47			-1.59	0.19	0.84	Open
48			-0.93	0.11	0.31	Open
49			-1.80	0.21	1.06	Open
50			-2.08	0.24	1.37	Open
51			14.05	0.44	1.58	Open
52			0.39	0.05	0.06	Open
53			12.53	0.39	1.28	Open
54			13.63	0.42	1.49	Open
55			0.81	0.10	0.35	Open
1			42.77	1.33	12.41	Open
56			-0.10	0.06	1.94	Open
57			0.11	0.06	1.06	Open

ACN 010 943 905 ABN 56 010 943 905

APPENDIX D
SEWERAGE RETICULATION
MASTER PLAN
DWG. 1208 OA Sewer





OCEAN BREEZE ESTATE STAGE 4A RESIDENTIAL SUBDIVISION AT JULAJI CLOSE COOYA BEACH

PROJECT DRAWINGS

PROJECT No. 1208

- C 01 EXISTING SITE PLAN.
- C 02 TYPICAL CROSS SECTION, PAVEMENT DATA, SET OUT AND INTERSECTION DETAILS.
- C 03 BULK EARTHWORKS PLAN.
- C 04 EARTHWORKS, ROADWORKS AND STORMWATER DRAINAGE PLAN.
- C 05 SOIL AND WATER MANAGEMENT PLAN.
- C 06 SEWERAGE RETICULATION PLAN.
- C 07 WATER RETICULATION PLAN.
- C 08 JULAJI CLOSE LONGITUDINAL AND CROSS SECTIONS.
- C 09 ROAD H LONGITUDINAL AND CROSS SECTIONS.
- C 10 STORMWATER DRAINAGE LONGITUDINAL SECTIONS, SET OUT DATA AND PIT SCHEDULE.
- C 11 SEWERAGE RETICULATION LONGITUDINAL SECTIONS, NOTES AND SET OUT.
- C 12 STORMWATER DRAINAGE CATCHMENT PLAN
- C 13 STORMWATER DRAINAGE CALCULATION SHEET

BRILEY CONSULTANTS

CONSULTING ENGINEERS

Ph. (07) 4054 3052 Mob 0400 543 052 Email: br85287@blgpond.net.au



RPS Australia East Pty Ltd ACN 140 292 762

10/9 Pioneet Cl CRAIGLIE QLD 4877 PO Box 355 MOSSMAN QLD 4873

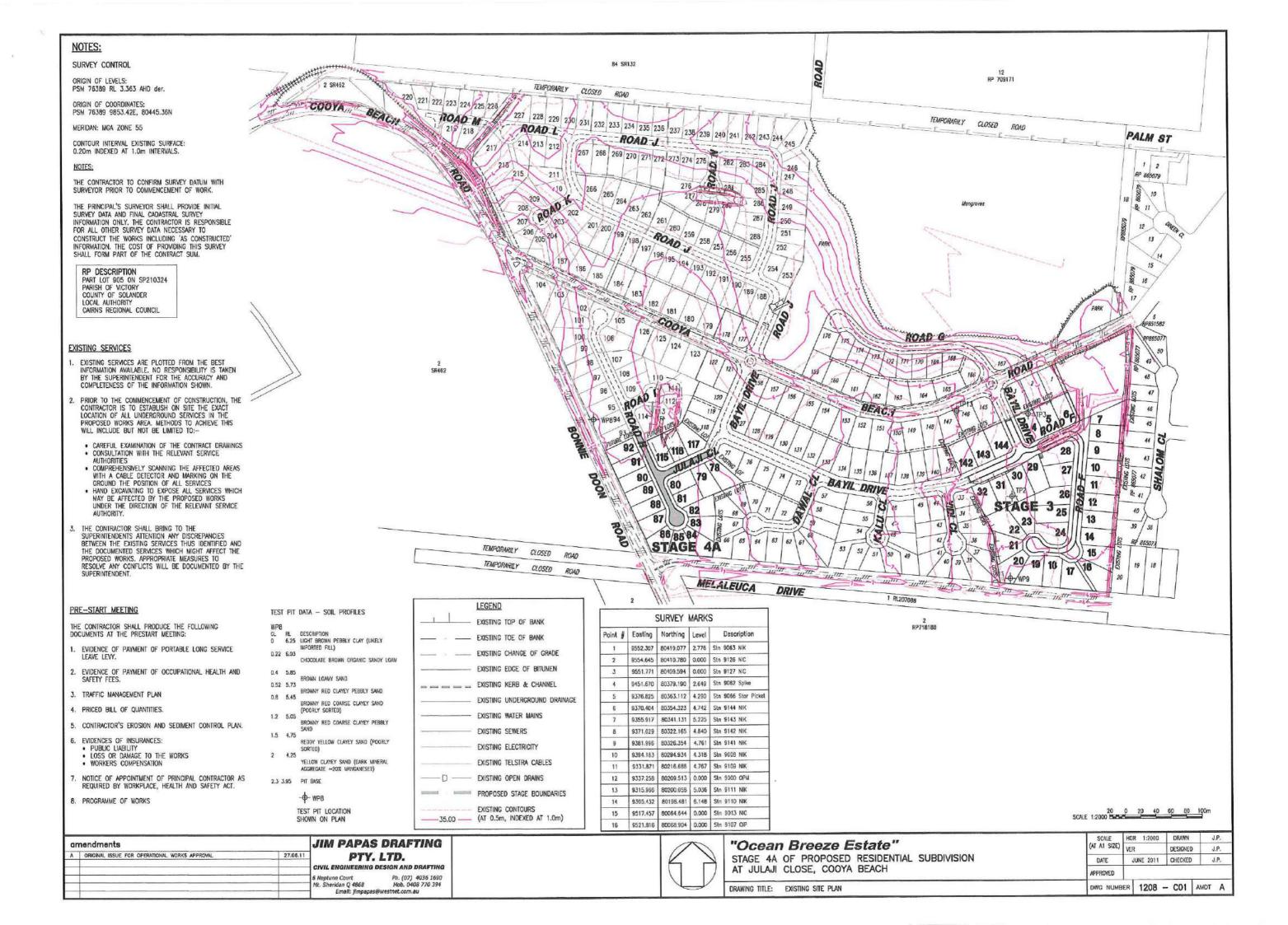
Unathersald reproduction to a transferred not

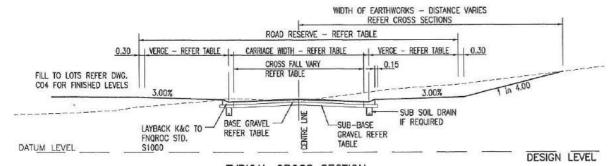
T +61 7 4098 114 F +61 7 4098 161

JIM PAPAS DRAFTING PTY. LTD.

CIVIL ENGINEERING DESIGN AND DRAFTING

5 Neptune Court Ph. (07) 4036 1690 Mt. Sheridan Q 4868 Mob. 0408 770 394 Emall: Jimpapas@westnet.com.au





TYPICAL CROSS SECTION JULUTI CLOSE & ROAD H

PAVEMENT NOTES

PAYEMENT NOTES

PROVISIONAL PAYEMENT DESIGN STATED HEREIN IS BASED ON A MINIMUM CBR UNDER SERVICE
CONDITIONS OF 7. PAYEMENT DESIGN IS SUBJECT TO REVISION ON BASIS OF CONFIRMATORY CBR
TESTS TAKEN AT THE TIME OF CONSTRUCTION. BASED ON THE INSITU CBR TEST RESULTS, THE FINAL PAVEMENT DESIGN SHALL APPROVED BY COUNCIL PRIOR TO CONSTRUCTION.
THE COMPLETED PAVEMENT DESIGN SHALL GENERALLY COMPLY WITH AUSTROADS OR DTMR PAVEMENT DESIGN MANUAL AS APPLICABLE.

SUBGRADE - COMPACT TO 100% SRDD. SHOULD ANY SOFT OR UNSUITABLE MATERIAL BE IDENTIFIED SEEK ADVICE OF THE SUPERINTENDENT.

SUBBASE SHALL CONSIST OF TYPE 2 SUBTYPE 2.3 PAVEMENT MATERIAL ('B' OR 'C' GRADED) COMPACTED TO 100% SRDD IN ACCORDANCE WITH SPECIFICATION. DEPTH OF PAVEMENT AS NOTED IN TABLE.

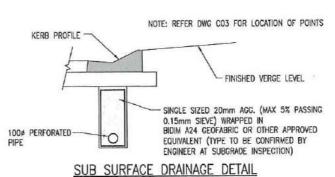
BASE SHALL CONSIST OF TYPE 2 SUBTYPE 2.2 PAVEMENT MATERIAL ("B" OR "C" GRADED) COMPACTED TO 100% SRDD IN ACCORDANCE WITH SPECIFICATION.
DEPTH OF PAVEMENT AS NOTED IN TABLE.

SEAL PAVEMENT AREAS WITH 300mm THICK ASPHALT "CRC10" AS DESCRIBED IN FNQROC DESIGN MANUAL CRC SPECIFIC CONDITIONS IN ACCORDANCE WITH THE SPECIFICATION. ASPHALT THICKNESS SHALL BE INCREASED TO 50mm WHERE SHOWN ON THE DRAWINGS.

ROAD NAME AND CHAINAGE	ROAD RESERVE WIDTH (m)	LHS VERGE WIDTH (m)	CARRIAGEWAY WIDTH (m) CROSSFALL (%)	RHS VERGE WIDTH (m)	SUBBASE (MIN. DEPTH mm)	BASE (MIN. DEPTI mm)
IULAJI CLOSE	17.00	5.00	7.00 (3%)	5.00	125	125
ROAD H	15.00	4.25	6.50 (3%)	4.25	125	125

	Julaji Close								
	CHAINAGE	EASTING	NORTHING	RADII	BEARING				
L#9	0.000 9.980	9024.428 9015.873	80277.156 80272.018		239'00'52" STRAIGHT 239'00'52" STRAIGHT				
C∦ 7	9.980 17.044	9015.873 9011.272	80272.018 80266.804	11.500 11.500	239'00'52" ARC 203'49'08" ARC				
L#10	17.044 28.451	9011.272 9006.666	80266.804 80256.368		203'49'08" STRAIGHT 203'49'08" STRAIGHT				
C# 8	28.451 34.087	9006.666 9003.486	80256.368 80251.755	15.000 15.000	203'49'08" ARC 225'20'51" ARC				
C# 9	34.087 39.355	9003.486 8999.172	80251.755 80248.780	15.000 15.000	225'20'51" ARC 245'28'05" ARC				
L#11	39.355 107.765	8999.172 8936.936	80248.780 80220.376		245'28'05" STRAIGHT 245'28'05" STRAIGHT				
	The state of the s		A CONTRACTOR OF THE PARTY OF TH						

Road H								
	CHAINAGE	EASTING	NORTHING	RADII	BEARING			
L#17	-15.000 0.000	8967.385 8961.157	80153.661 80167.307		335*28'05" STRAIGHT 335*28'05" STRAIGHT			
L#18	0.000 117.769	8961.157 8912.259	80167,307 80274,445		335'28'05" STRAIGHT 335'28'05" STRAIGHT			
L#19	117.769 250.507	8912.259 8857.147	80274.445 80395.201		335'28'05" STRAIGHT 335'28'05" STRAIGHT			
C# 11	250.507 266.163	8857.147 8856.984	80395.201 80410.405	18.750 18.750	335'28'05" ARC 23'18'31" ARC			
L#20	266.163 284.144	8856.984 8864.099	80410,405 80426,918		23'18'31" STRAIGHT 23'18'31" STRAIGHT			
L#21	284.144 299.270	8864.099 8870.084	80426.918 80440.810		23'18'31" STRAIGHT 23'18'31" STRAIGHT			



(IF REQUIRED) N.T.S.	

Point #	Easting	Northing	Level	Description	
601	8934.033	80233.891	5.898	EC	
602	8936.378	80230.637	5.873	EC	
603	8939.790	80228.528	5.774	EC	
604	8943.749	80227.885	5.655	EC	
605	8947.653	80228.807	5.571	EC	
606	8950.327	80222.948	5.571	EC	
607	8947.073	80220.603	5.662	EC	
608	8944.964	80217.191	5.802	EC	
609	8944,322	80213.232	5.929	EC	
610	8945.243	80209.328	5.979	EC	
611	8956.765	80184.084	6.080	EC	
612	8958.196	80181.596	6.092	EC	
613	8960.068	80179.420	6.105	EC	
614	8962.314	80177,632	6.117	EC	
615	8964.854	80176.296	6.129	EC	
616	8967.898	80174.309	6.144	EC	
617	8969.999 80171.342		6.160	EC	
618	8970.871	80167.651	6.176 6.192	EC	
619	8970.263	80163.908		EC	
620	8968.269	80160.682	6.209	EC	
621	8965,193	80158.464	6.226	EC	
622	8961.502	80157.593	6.209	EC	
623	8957.758	80158.200	6.193	EC	
624	8954.532	80160.194	6.176	EC	
625	8952.314	80163.271	6.160	EC	
626	8951.450	80166.802	6.145	EC	
627	8951.944	80170.404	6.129	EC	
628	8952.599	80173.199	6.117	EC	
629	8952.720	80176.066	6.105	EC	
630	8952.302	80178.906	6.093	EC	
631	8951.361	80181.617	6.080	EC	

NOTE: EC = EDGE OF CHANNEL = EDGE OF BITUMEN

100	R=10.280 ARC=16.148 (4x4.037) LOT 115
603 603 603 603 603 603 603 603 603 603	S 3 JULY CLOSE
LOT 90	NOTE: SHADED AREA INDICATES THE AREA OF ASPHALT 50mm THICK
LOT 89	R=10.280 ARC=16.148 (4x4.037) LOT 80

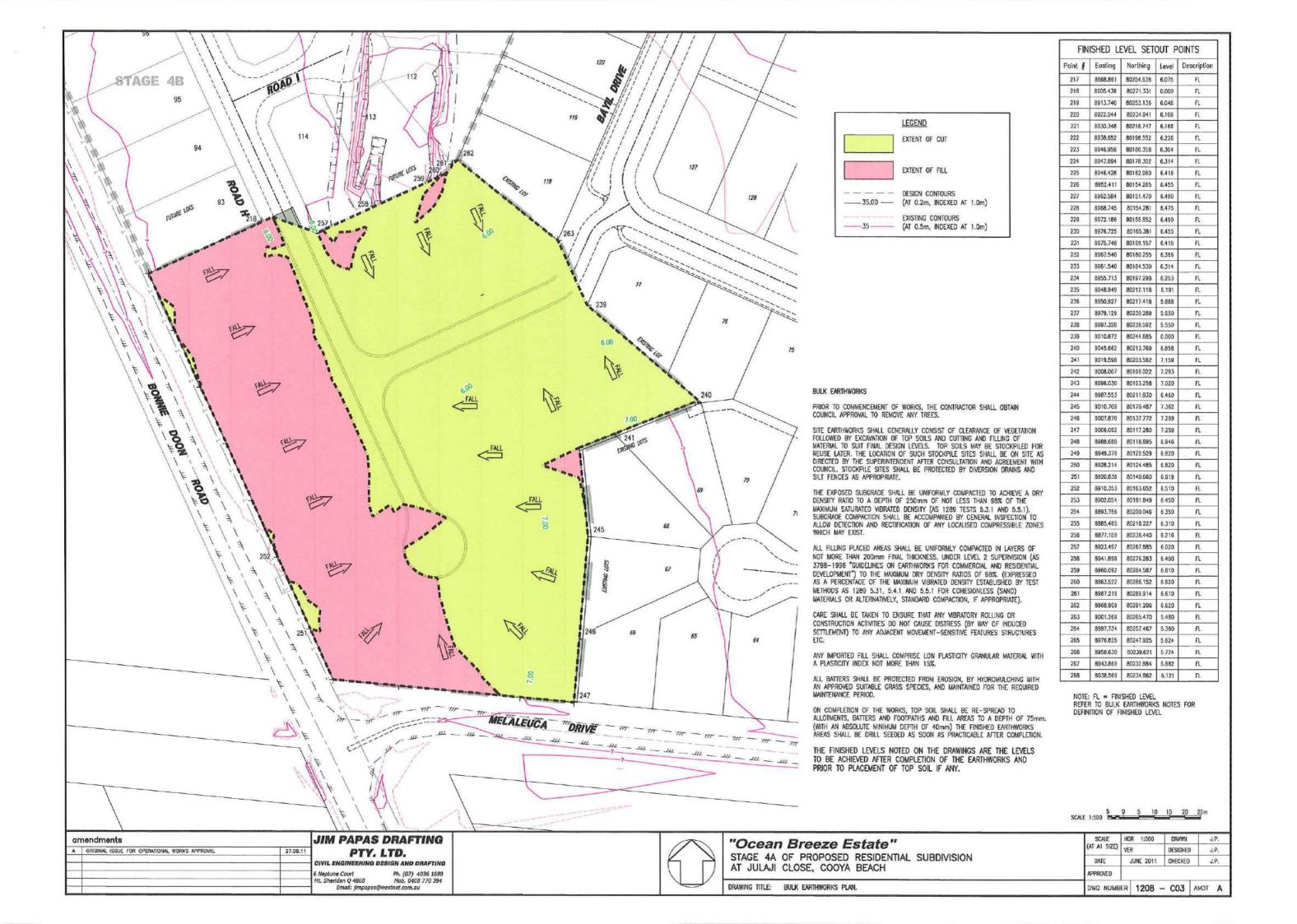
/ # 17x. # /
CH 12 LOT 81 R=15.28
ARC=11.498
10T 00 \ h(1-)(1 0 MIN)
630 R=15.28 ARC=11.498
ARC-11.498 (4)2.875) 629
LOT 82
627-
ARC=7,314 (2x3,657) 626-111 CH CH CH 600 CH O CH CH 635
111111111111111111111111111111111111111
625 The first lot 83
624
623
622 R=9.72 LOT 84
LOT 86 (8x3.817) CH -151
LOT 85

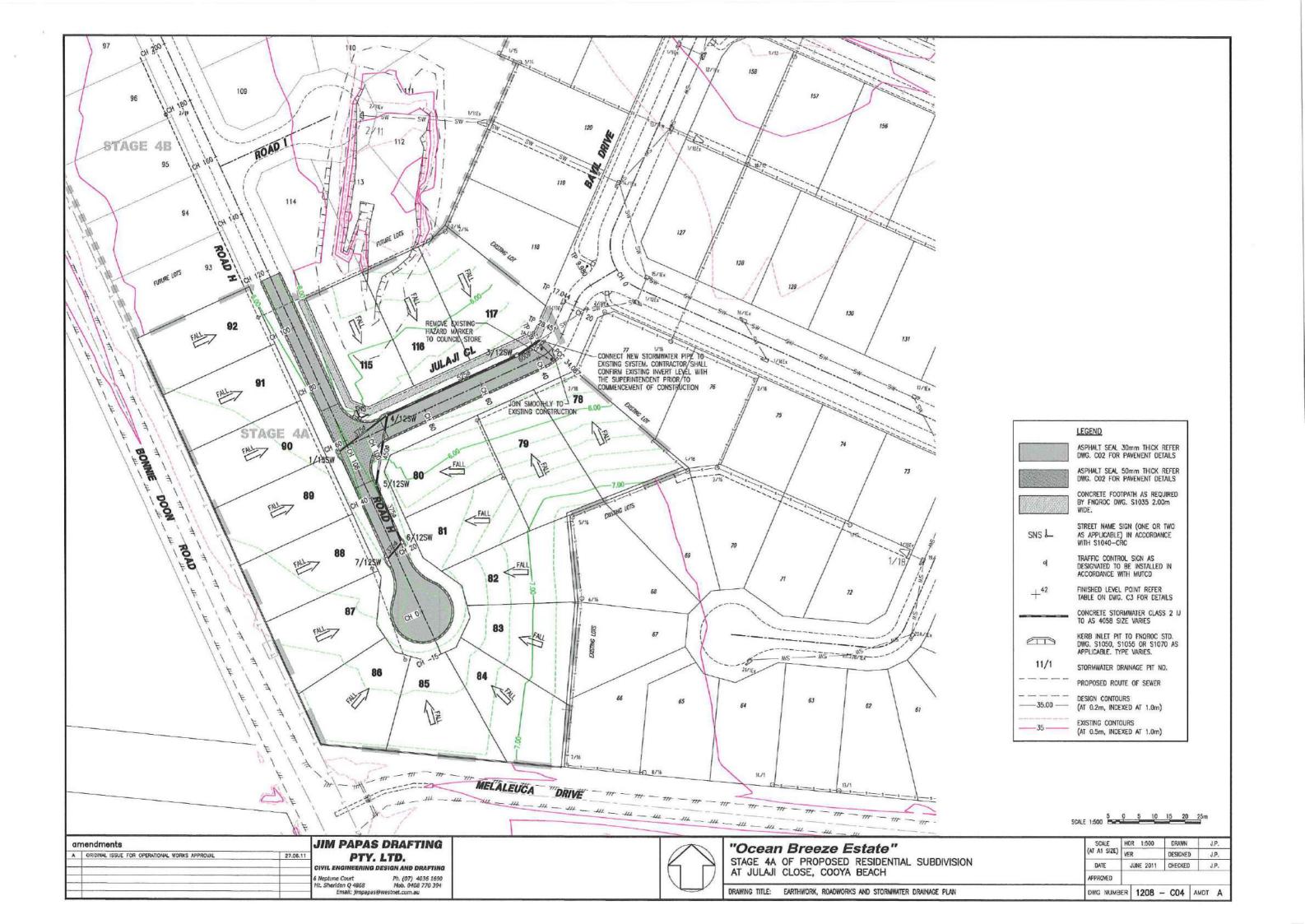
INTERSECTION DETAILS SCALE: 1:200

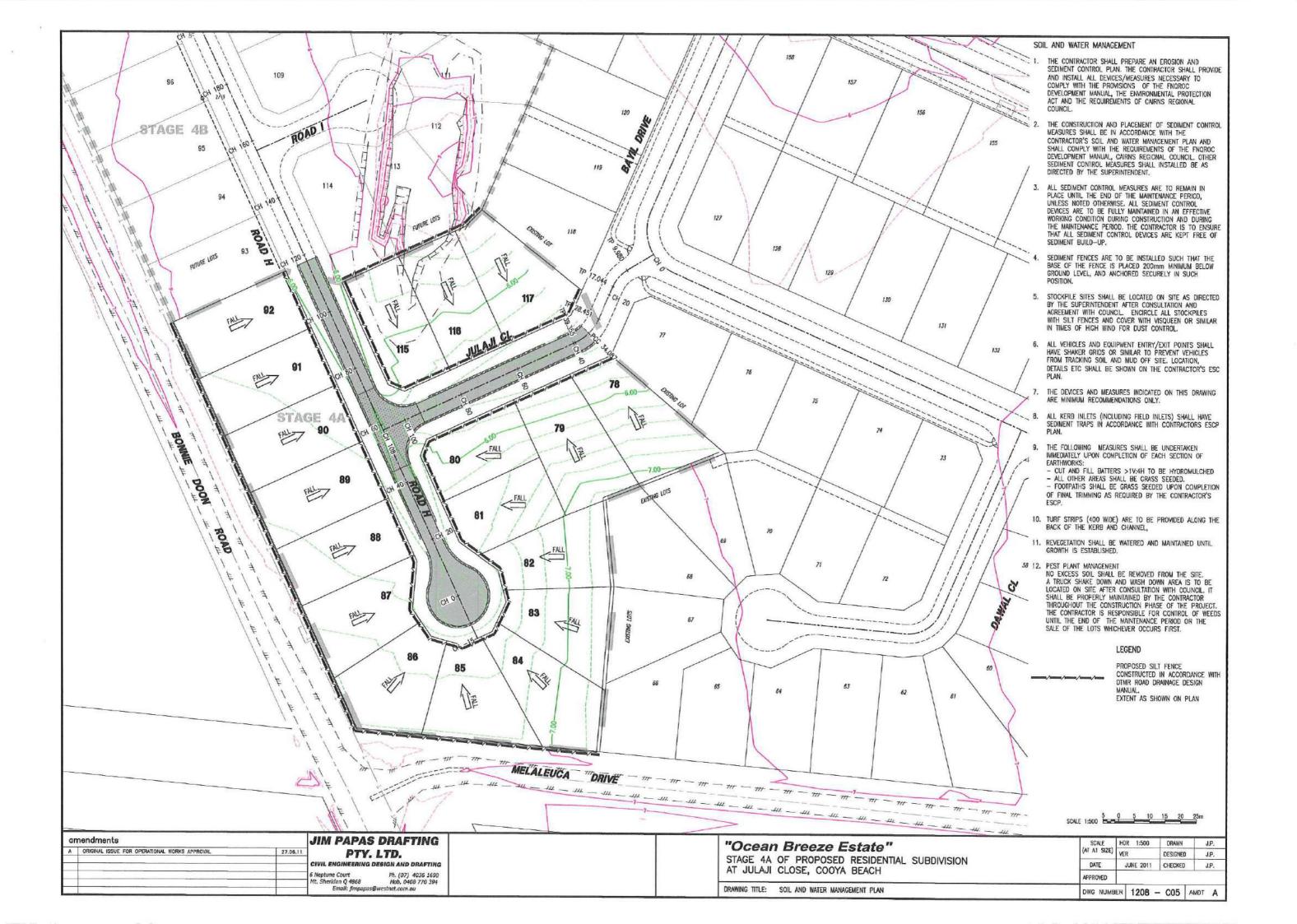
> SCALE 1:100 1.0 0 1.0 2.0 3.0 4.0 5.0m SCALE 1:200 2.0 0 2.0 4,0 6.0 8,0 10.0m

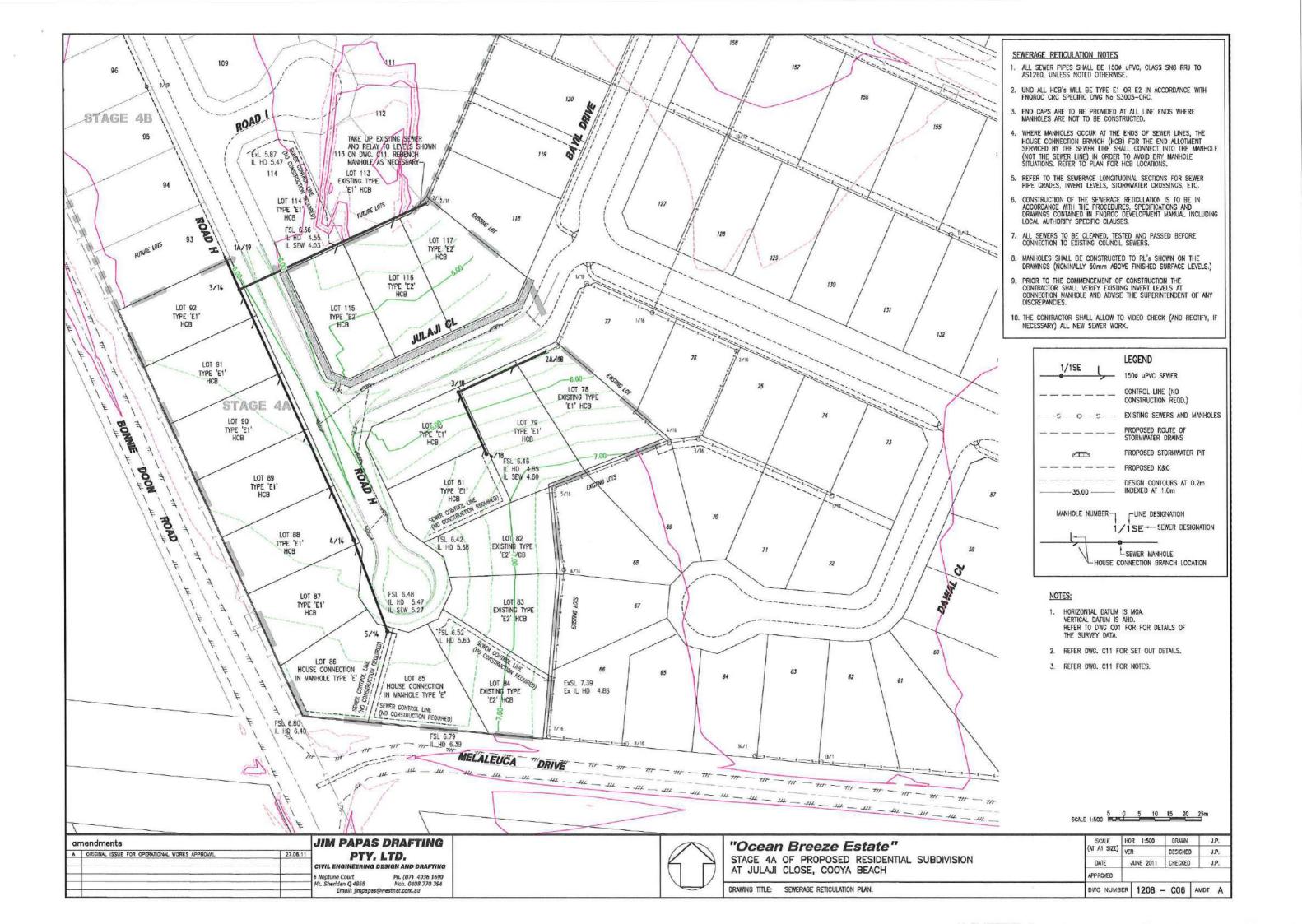
an	nendments		JIM PAPAS	DRAFTING
A	ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL	27.06.11	PTY.	LTD.
			6 Neptune Court Mt. Sheridan Q 4868	Ph. (07) 4036 1690 Mob. 0408 770 394 Dwestnet.com.au

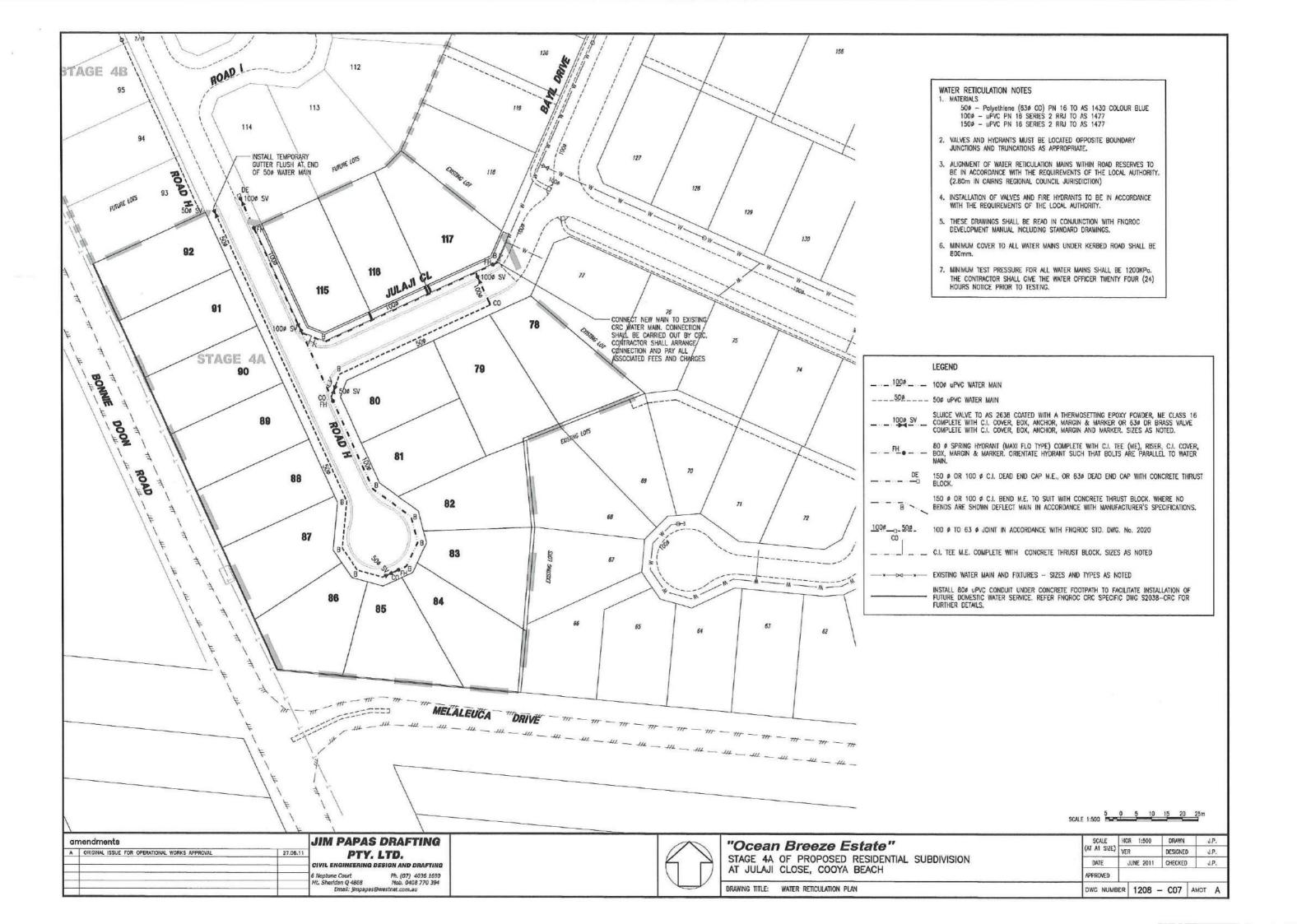
"Ocean Breeze Estate"		HOR 1:200/100	DRAWN	J.P.	4)
		VER 1:100	DESIGNED	J.P.	
STAGE 4A OF PROPOSED RESIDENTIAL SUBDIVISION	DATE	JUNE 2011	CHECKED	J.P.	
AT JULAJI CLOSE, COOYA BEACH	APPROVED				
DRAWING TITLE: TYPICAL CROSS SECTION, PAVEMENT DATA, SET OUT AND INTERSECTION DETAILS.	DWG NUMB	ER 1208 -	- C02	AMDT	Α

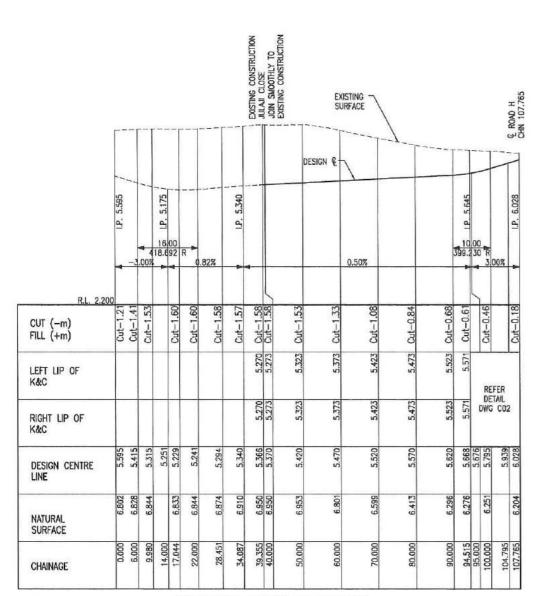




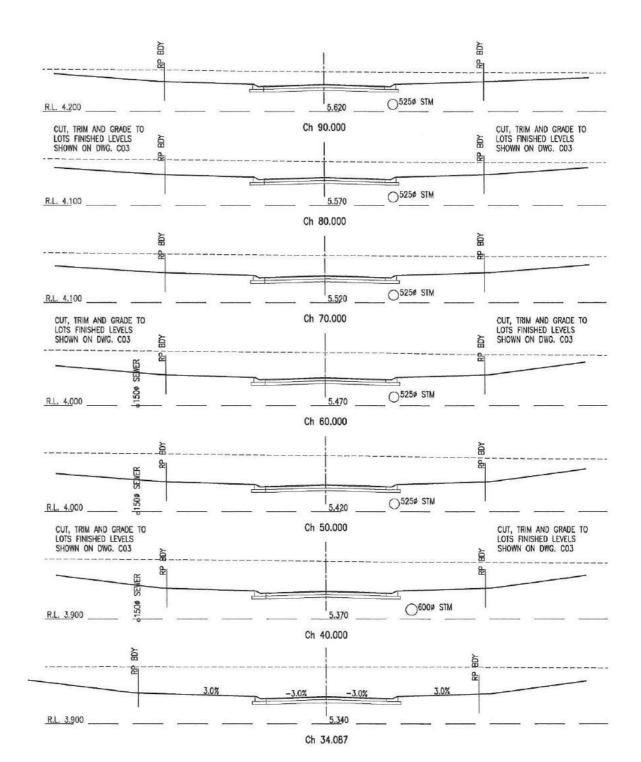








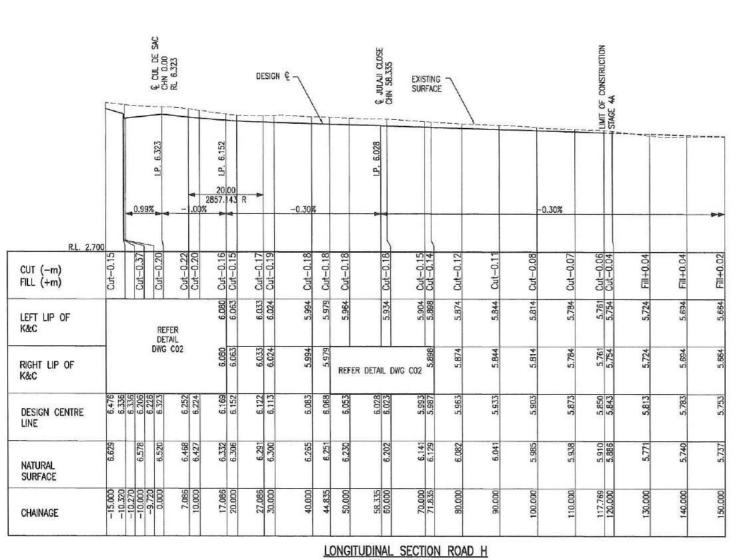
LONGITUDINAL SECTION JULAJI CLOSE
SCALES: HOR. 1:500
VER: 1:50



CROSS SECTIONS JULAJI CLOSE SCALES: HOR. 1:100 VER: 1:100

ar	nendments		JIM PAPAS DRAFTING	
A	ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL	27.06.11	PTY. LTD.	
			CIVIL ENGINEERING DESIGN AND DRAFTING	
			6 Neptune Court Ph. (07) 4036 1690	
			Mt. Sheridan Q 4868 Mob. 0408 770 394 Email: jimpapas@westnet.com.au	

"Ocean Breeze Estate"	SCALE HOR 1:500/100 DRAWN J.P.
	(AT A1 SIZE) VER 1:50/100 DESIGNED J.P.
STAGE 4A OF PROPOSED RESIDENTIAL SUBDIVISION	DATE JUNE 2011 CHECKED J.P.
AT JULAJI CLOSE, COOYA BEACH	APPROVED
DRAWING TITLE: JULAJI CLOSE - LONGITUDINAL AND CROSS SECTIONS	DWG NUMBER 1208-COB AMDT A



LONGITUDINAL SECTION ROAD H SCALES: HOR. 1:500 VER: 1:50

SHOWN ON DWG, C03	SEWER	Bdy					
R.L. 4.400	0150	- 85 - 18			5.850		
				Ch 1	117.769		
	8	Ī	8.398		-	7.808	7
	S SWER	Bdy					Bdy
R.L. 4.500	¢150ø	8			5.903		8
FILL, TRIM AND GRADE TO	1			Ch 1	100.000		
LOTS FINISHED LEVELS SHOWN ON DWG. CO3		Ī	8.066		-	7.953	→
	SEWER	Bdy			+====		Bdy
R.L. 4,500	p150¢	-87 B			5.963		95 80
			And the same of th	Ch	80.000		
	85	Ĩ	7.928	233	-	8.005	
	SEWER	Bdy					Pdy Bdy
R.L. 4,500	o150¢	89 BB	t-		5.987		8 8
		-		- Ch	71.835		
FILL, TRIM AND GRADE TO LOTS FINISHED LEVELS		Ĩ	7.804	OII	1 1,000		
SHOWN ON DWG. CO3	SEVER					JULAJI CLOSE	
DI 4600	01500	RP Bdy			0.007		2764 STU
R.L. 4.600	0	<u>œ</u>			6.023) 3/3v 3im
FILL, TRIM AND GRADE TO LOTS FINISHED LEVELS		4	7.853	Ch	60.000	8.210	 ►
SHOWN ON DWG. CO3	SEWER				Ĭ		
	o150¢ S	Bdy				=1	Bdy
R.L. 4.600	0	&			6.068		<u></u>
			7.855	Ch	44.835	8.208	500 0 01
	SEWER		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		4	0.200	
· · · · · · · · · · · · · · · · · · ·	o150¢ Si	Bdy	THE		1	=1	BB
R.L. 4.600	-6	_₽			6.083	O 3750 STM	<u> </u>
FILL, TRIM AND GRADE TO	2			Ch	40.000		
LOTS FINISHED LEVELS	SEWER	Ĩ	8.083		-	8.389	
SHOWN ON DWG, CO3	<u> </u>	ð			+		Bdy
R.L. 4.700	o150¢	RP Bdy	0.3	75ø STM	6.152		& ₩
					20.000		
	8	1	8.129		4	8.453	
	SEWER						
0. 4.700	o150¢	RP Bdy					RP Bdy
R.L. 4.700		<u> </u>			6.169		
WER BODY				Cn	17.086		
3.0% SEWER							
- S-							5,0/6
R.L. 4.900					6.323		
				Ch	0.000		

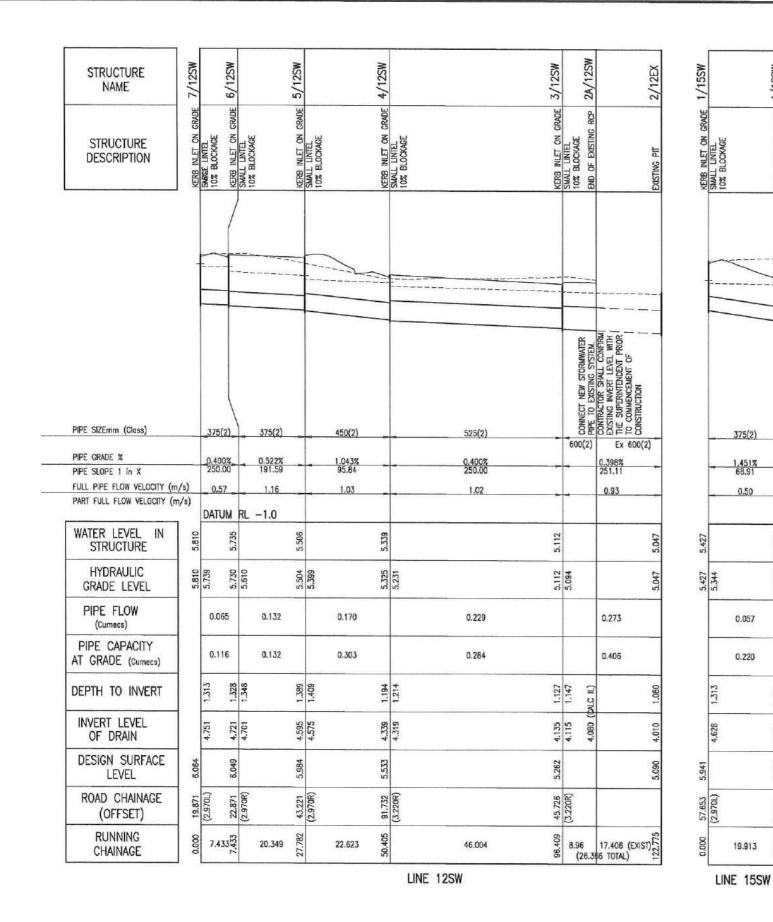
CROSS SECTIONS ROAD H SCALES: HOR. 1:100

VER: 1:100

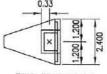
SCALE 1:50 0.5 0 0.5 1.0 1.5 2.0 2.5m SCALE 1:500 5 0 5 10 15 20 25.0m

an	nendments		JIM PAPAS	DRAFTING
A	ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL	27.05.11	PTY.	LTD.
	W-12		CIVIL ENGINEERING L	ESIGN AND DRAFTING
			6 Neptune Court Mt. Sheridan Q 4868	Ph. (07) 4036 1690 Mob. 0408 770 394
			Emall: Jimpapase	

"Ocean Breeze Estate"	SCALE (AT AT SIZE)	HOR 1:500/100 VER 1:50/100	DRAWN DESIGNED	J.P.
STAGE 4A OF PROPOSED RESIDENTIAL SUBDIVISION AT JULAJI CLOSE, COOYA BEACH	DATE APPROVED	JUNE 2011	CHECKED	J.P.
DRAWING TITLE: ROAD H - LONGITUDINAL AND CROSS SECTIONS	DWG NUMBI	R 1208 -	C09	AMDT A

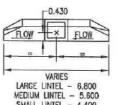


		PIT	SC	HEDULE					
PIT		INTE	RNAL	INL	ET	OUT	LET		PIT
No.	TYPE	WIDTH	LEN.	DIA.(CL)	INV R.L.	DIA.(CL)	INV R.L.	F.S.L.	DEPTH
7/12SW	KERB INLET ON GRADE SMALL LINTEL 10% BLOCKAGE	835	930			375(2)	4.751	6.064	1.31
6/12SW	KERB INLET ON GRADE LARGE LINTEL 10% BLOCKAGE	835	930	375(2)	4.721	375(2)	4.701	6.049	1.35
5/12SW	KERB INLET ON GRADE SMALL LINTEL 10% BLOCKAGE	835	930	375(2)	4.595	450(2)	4.575	5.984	1.41
1/15SW	KERB INLET ON GRADE SMALL LINTEL 10% BLOCKAGE	835	930			375(2)	4.628	5.941	1.31
4/12SW	KERB INLET ON GRADE SMALL LINTEL 10% BLOCKAGE	835	930	375(2) 450(2)	4.339 4.339	525(2)	4.319	5.533	1.21
3/12SW	KERB INLET ON GRADE SMALL LINTEL 10% BLOCKAGE	835	930	525(2)	4.135	600(2)	4.115	5.262	1.15



KERB INLET ON SMALL LINTEL 10% BLOCKAGE

FIELD INLET TYPE A



MEDIUM LINTEL - 5.600 SMALL LINTEL - 4.400 KERB INLET PIT IN SAG

FLOW X 1.645 0.430

LARGE LINTEL - 6.800 SMALL LINTEL - 4.400 KERB INLET PIT ON GRADE

NOTES:

SET OUT POINT IS CENTRE OF GRATE

WIDTH IS DIMENSION PERPENDICULAR TO PRECAST BACKSTONE (i.e. TYPICALLY PERPENDICULAR TO THE LINE OF THE KERB AND

LENGTH IS DIMENSION PARALLEL TO THE LINE OF THE KERB AND CHANNEL,

INSTALL 2.0m SUB SOIL DRAIN AS REQUIRED BY FNORCC, DWGS,

PIPE LENGTHS SHOWN ARE MEASURED FROM CENTRE OF GRATE TO CENTRE OF GRATE

ALL STORMWATER DRAIN PIPES SHALL BE R.C. PIPES CLASS 2 1J TO AS 4058 FSL NOTED IS THE EDGE OF THE KERB AND CHANNEL PERPENDICULAR TO THE SETOUT POINT.

UNTEL LENGTHS NOTED INCLUDE TRANSITION LENGTHS.

STORMWATER DRAINAGE SET OUT DETAILS

ST	ORMWAT	ER SETO	UT P	STAIC
Point #	Easting	Northing	Level	Description
420	8999,368	80254.416	6.911	2A/12SW
421	8991.860	80249.455	5.262	3/12SW
422	8950,008	80230.355	5.533	4/125W
423	8946.305	80208.037	5.984	5/12SW
424	8954.754	80189,525	6,049	6/12SW
425	8949.813	80183,972	6.064	7/125W
426	8934,126	80218.343	5.941	1/15SW

ar	mendments		JIM PAPAS	DRAFTING
A	ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL	27.06.11	PTY,	LTD. DESIGN AND DRAFTING
			6 Neptune Court Mt. Sheridan Q 4868 Email: Jimpapass	Ph. (07) 4036 1690 Mob. 0408 770 394 Dwestnet.com.au

"Ocear	Breeze E	state"	
	OF PROPOSED CLOSE, COOYA		SUBDIVISION

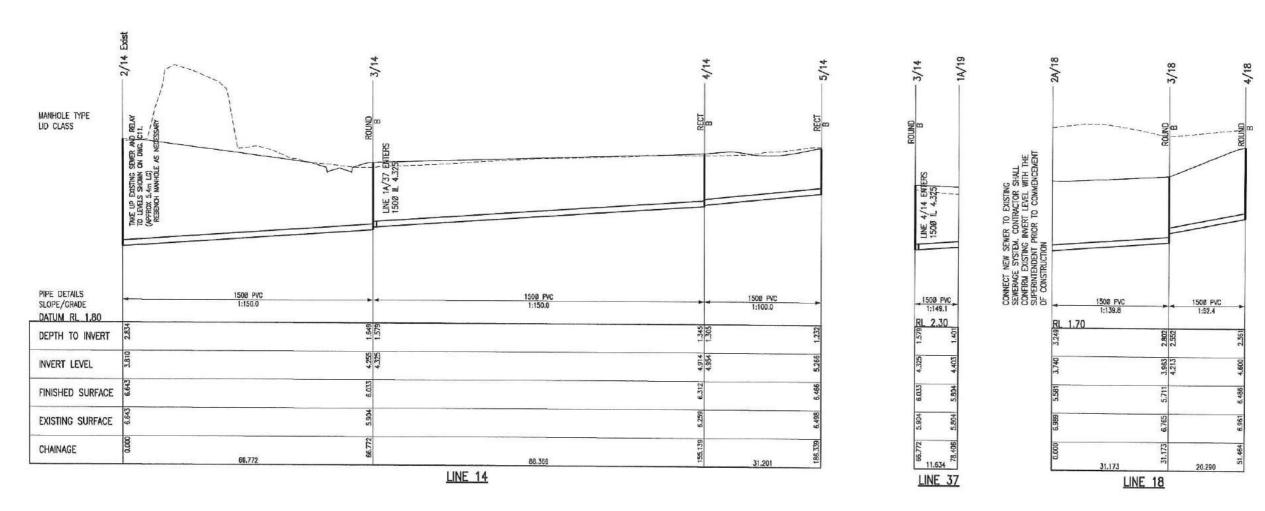
DRAWING TITLE: STORMWATER DRAINAGE LONGITUDINAL SECTIONS, SET OUT DATA AND PIT SCHEDULE

DWG NUMB	ER	1208 -	- C10	AMDT A
APPROVED				
DATE	JL	INE 2011	CHECKED	J.P.
(AT A1 SIZE)	VER	1:50	DESIGNED	J.P.
SCALE	HUK	1:500	DRAWN	J.P.

SEWER SETOUT POINTS											
Point #	Easting	Northing	Level	Description							
520	8969.024	80289.213	6.620	2/14							
521	8908.279	80261.489	6.083	3/14							
522	8944.969	80181.099	6.362	4/14							
523	8955.725	80151.811	6.516	5/14							
524	8903,449	80272.072	5.800	14/19							
525	9007,383	80241.536	5.631	2A/18							
526	8979.024	80228.593	5.761	3/18							
527	8987.449	80210.134	6.536	4/18							

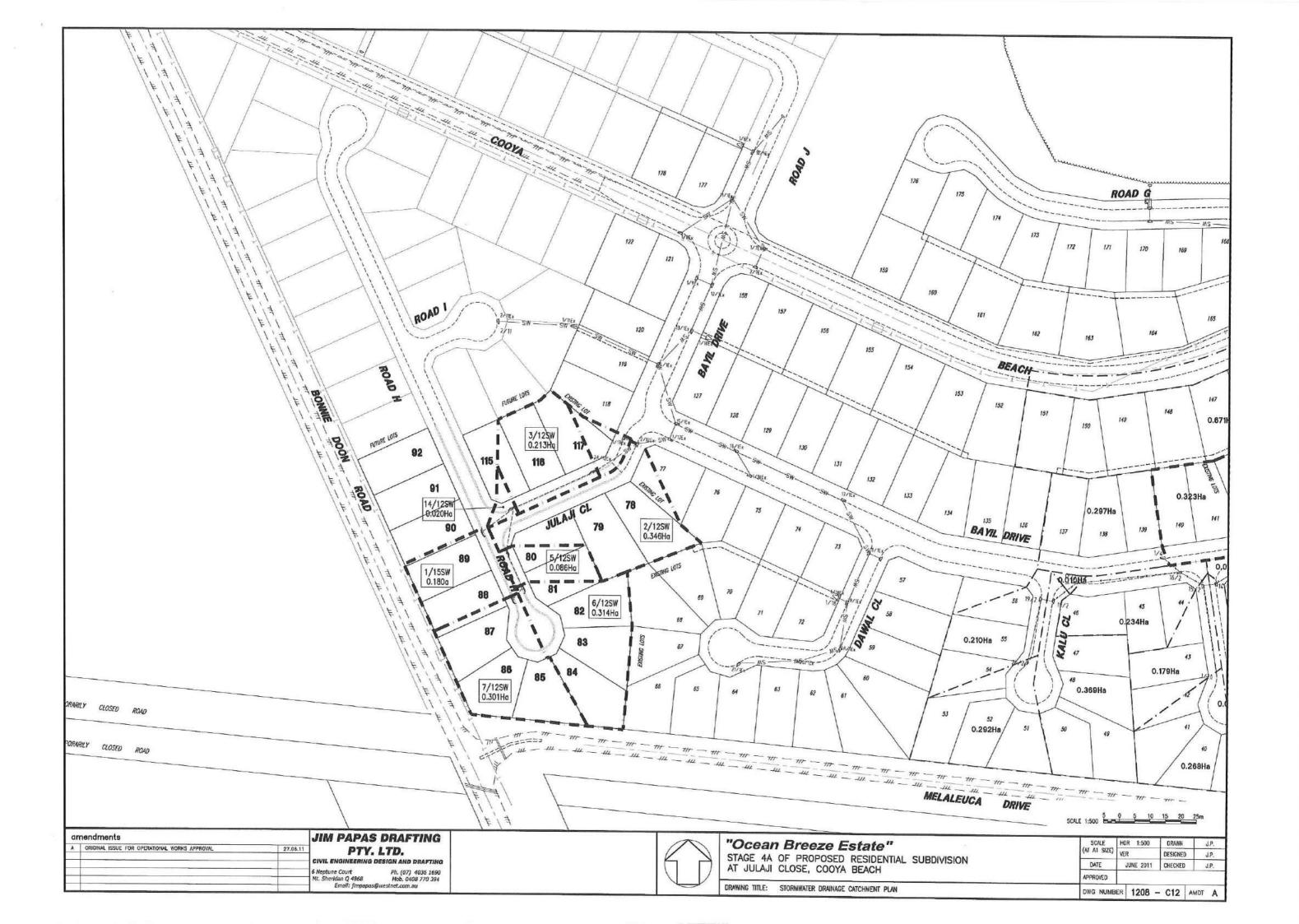
SEWERAGE RETICULATION NOTES

- ALL SEWER PIPES SHALL BE 1500 uPVC, CLASS SN8 RRJ TO AS1260, UNLESS NOTED OTHERWISE.
- UNO ALL HCB's WILL BE TYPE E1 OR E2 IN ACCORDANCE WITH FNQROC CRC SPECIFIC DWG No S3005-CRC.
- END CAPS ARE TO BE PROVIDED AT ALL LINE ENDS WHERE MANHOLES ARE NOT TO BE CONSTRUCTED.
- 4. WHERE MANHOLES OCCUR AT THE ENDS OF SEWER LINES, THE HOUSE CONNECTION BRANCH (HCB) FOR THE END ALLOTMENT SERVICED BY THE SEWER LINE SHALL CONNECT INTO THE MANHOLE (NOT THE SEWER LINE) IN ORDER TO AVOID DRY MANHOLE SITUATIONS. REFER TO PLAN FOR HCB LOCATIONS.
- REFER TO THE SEWERAGE LONGITUDINAL SECTIONS FOR SEWER PIPE GRADES, INVERT LEVELS, STORMWATER CROSSINGS, ETC.
- CONSTRUCTION OF THE SEWERAGE RETICULATION IS TO BE IN ACCORDANCE WITH THE PROCEDURES, SPECIFICATIONS AND DRAWINGS CONTAINED IN FNOROC DEVELOPMENT MANUAL INCLUDING LOCAL AUTHORITY SPECIFIC CLAUSES.
- ALL SEWERS TO BE CLEANED, TESTED AND PASSED BEFORE CONNECTION TO EXISTING COUNCIL SEWERS.
- MANHOLES SHALL BE CONSTRUCTED TO RL'S SHOWN ON THE DRAWINGS (NOMINALLY 50mm ABOVE FINISHED SURFACE LEVELS.)
- PRIOR TO THE COMMENCEMENT OF CONSTRUCTION THE CONTRACTOR SHALL VERIFY EXISTING INVERT LEVELS AT CONNECTION MANHOLE AND ADVISE THE SUPERINTENDENT OF ANY DISCREPANCIES.
- THE CONTRACTOR SHALL ALLOW TO VIDEO CHECK (AND RECTIFY, IF NECESSARY) ALL NEW SEWER WORK.



SCALE 1:50 5 0 0.5 1.0 1.5 2.0 2.5m SCALE 1:500 5 0 5 10 15 20 25.0m

amendments		JIM PAPAS DRAFTING	"Ocean Breeze Estate"	SCALE	HOR 1:500	DRAWN	J.P.
A ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL	27.06.11	PTY. LTD.		(AT AI SIZE)			-
		CIVIL ENGINEERING DESIGN AND DRAFTING	STAGE 4A OF PROPOSED RESIDENTIAL SUBDIVISION AT JULAJI CLOSE, COOYA BEACH	DATE	JUNE 201	CHECKEO	J.P.
		6 Neptune Court Ph. (07) 4036 1690 Mt. Sheridan Q 4868 Mob. 0408 770 394	THE GODAL GEOSE, GOOTA BEACH	APPROVED			
		Email: fimpapas@westnet.com.au	DRAWING TITLE: SEWERAGE RETICULATION LONGITUDINAL SECTIONS, NOTES AND SET OUT DATA.	DWG NUMB	ER 1208	- C11	AMDT A



	LOCATI	ION	-51				-CATCHME	ENT RUI	NOFF					INLET	DESIGN										DRAIN	DESIGN				_			HE	ADLOSS	SES		-	-	-		1	PART FULL	_			_			
-	-	-		tc	1	1	A	-	Q	-	-			_							te	1		Qt Q	m Q	s Q	o L	S		٧	t				hu	kl	hi	bw	hw	SI		PART FULL	-	T	-		_		_
DESIGN A.R.I.	DRAIN SECTION		SUB-CATCHMENTS CONTRIBUTING	SUB-CATCHMENT TIME OF CONCENTRATION	RAINFALL	COEFFICIENT OF RUNOFF	SUB-CATCHMENT AREA	SUM OF CONTRIBUTING	SUB-CATCHMENT	FLOW PAST DEPARTMENT	FLOW IN K&C	ROAD GRADE AT INLET	FLOW WIDTH	AT INVERT		dg x Vg INLET NUMBER	INLET TYPE	FLOW INTO INLET	WIDTH OF FLOW D/S OF INLET	8	CONCENTRATION	RAINFALL INTENSITY	EQUIVALENT AREA	TOTAL FLOW	FLOW CAPACITY MAJOR	SURFACE FLOW	REACH LENGTH	PIPE GRADE	PIPE / BOX DIMENSIONS	PLOW VELOCITY FULL (PIPE GRADE VELOCITY)	DF FLOW	STRUCTURE RATIOS FOR 'K' VALUE CALCULATIONS	VELOCITY HEAD	U/S HEADLOSS COEFFICIENT	PIPE STRUCTURE	HEADLOSS	LATERAL PIPE STRUCTURE HEADLOSS		HANGE IN W.S.E	FRICTION SLOPE	FRICTION	овятн увлосту	OBVERT LEVELS U/S RL D/S RL	RAIN SECTION H.G.L. /S RL. /S RL	/s HGL	SE	SURFACE OR K&C INVERT LEVEL		manuscraft N.
ears				mîn	mm/t	N	Ha H	la H	a cume	cscume	cscume	18	m	m n	n/secm	/sec		cumec	s m	cumecs	min	mm/h	Ha cur	necscum	ecscum	ecscume	ecs m	7,		m/sec			m	1	m	m	m	20	_				-	1	3	*	-		- 0
5 7/1	25W 7/125	WZCI	7/12SW	15.00	139	0.76	0.301 0.2	229 0.2	29 0.08	8 0.00	0.088	0.55	2,512	0.095	0.69	0.07 7/125	W 4	0.065	1.347	0.023		139 0 220 0		177 1.8	23 0.1	12 0.06	65 7.433	0,40	375(2)	0.57	0.12	Qq 0.065 Qo 0.065 Do 375.000		4.25		m	***	1.00	m	0.13		m m/se		m	m	m	m		
														. 1																1		CHRT 32: Vo2/2gDo 0.04 H/Do Kg side flow 4.25 end flow 3.40	0.017	4.20	0.071			1.20	0.071	0.13	0.009		5.132 5.102	5.739 5.730	5.810	5.810	6.064	0.254	7/12
100	10 5/1	125W	/125W;6/12 SW	15.00	220	0.96	0.314 0.3	301 0.3	0.18	4										0/1234	13.12	220 0	.550		(Pipe flo	w= bum i	upstr otte	n flows)		(1.15)		0g 0.068 Qo 0.132 Do 375,000 Angle 67 Chart 43 5/Do 2.5 chert Dv/Do 1.00 NO 1.35 No.5. 1.93 Qv/Qo 0.49 Cg 1.01 K 1.93 S/Do 3.0 NO 1.33 No.5 1.96 K 1.66 S/Do 2.5 NO 1.35 No.5 1.93 K 1.93	0.059	1.75	0.120	S/Do 3	rol for S 42 5.0 KO 1 5.5 KO 1 val for S	/Do 2 7	71 Kw 1 5 1.64 5 1.82	K 1.64	0.106		5.082 4.976	5.610 5.504	5,730	5.735	6.049	0.314	8/12
	to 4/1		/125W;6/12 5W;5/125W																	ZFIZEK	13,41	210	.673		(Pipe 1io	w= Sum (upstr otte	n flows)		(1.85)		Angle 34 Chart 39 S/Do 2.5 chart Du/Do 0.83 KO 1.90 KO.5 1,79 Qu/Qo 0.77 Cg 0.53 K 1.84	0.054	1.94	0.105	Interp	vel for S 38 .5 KO 1 .0 KO 2 vel for S	1.99 /00 2 0 .84 KQ.5	0.107 04 Kw 1 5 1.71 5 1.83	0.33 .99 K 1.77 K 1.95	0.074		5.032 4.796	5,399 5,325	5.504	5.506	5.984	0.478 5	5/12
100	to 4/1		1/105#	15.00	220	0.96	0.180 0.1	173 0.1	73 0.10	8 0.02	3 0.076	0.30	2.690	0,101	0.53	0.05 1/155	W 4	0.057	1.426	0.019	15.00	139 220 0	137 0.	106 3.5	62 0.0 (Fi	49 0.05 ipa (low=	57 19.91 Grate flo	3 1.45 w)	375(2)	0.50 (1.93)	0.33	S/Do 2.0 KO 2.11 KO.5 1.90 K 2.00 Qg 0.057 Qo 0.057 Do 375.000 CHRI 32: Yo2/2gbo 0.03 H/Do Kg side flow 6.47 and flow 4.76	0.013	6.47	0.083	Aug. p	-		-	0.10	0.019		5.009 4.720	5.344 5.325	5.427	5.427	5.941	0.514 1	1/15
100	to 3/1	125W SW	/12SW;6/12 N;5/12SW;1/ 5SW;4/12SW	15.00	139 220	0.76 0.96	0.020 0.0 0.020 0.0	015 0.0 019 0.0	15 0.00 19 0.01	6 0.000	0.006	1.00	0.499	0.035	0.50	0.02 4/125	W 4	0.005		0.001 3/125W	15.78 15.78	136 0 216 0	.685 O.:	519 2.8	66 0.2 (Pipe flor	90 0.22 v= Sum (29 46.00 upstr atte	4 0.40 n flows)	525(2)	1.02 (1.27)	0.75	Qg 0.005 Qo 0.229 Do 525.000 Routine 2.24 John Pipes: 1/155W end 5/125W Yell 0.505 Wel2 1.055 E Die 555 Angle 134 Flow 0.224 Angle 45 Chort 39 S/Do 2.5 chart Do/Do 1.06 KO 1.77 KO.5 1.95 Qo/Qo 0.98 Cg 0.06 K 1.78	0.053	1.76		S/Do 1 Interp CHART S/Do 2 S/Do 1	.0 KO 6 .5 KO 2 rol for S .38 .0 KO 1 .5 KO 1	96 KO 3 36 KO 3 /Do 1 9 73 KO 3 89 KO 3	5 2.19 5 2.65 11 Kw 2 5 1.70	C 1.73	0.119		4.853 4.659	5.231 5.112	5.325	5.339	5.533	0.194 4	4/12
100	to 2/1	12Ex 59	/125W;6/12 N;5/125W;1/ 55W;4/125W; 3/125W	15.00	220	0.96	0.213 0.2	204 0.2	04 0.12	5 0.00	0.084	0.58	2,159	0.085	0.65	0.06 3/125	m 4	0.049	1.065	0.015	16.53	212 1	.069 O.	630 2.8	66 0.3 (Pipe flor	57 0.27 #= Sum i	73 26.36 upstr atte	6 0.40 n flows)	600(2)	0.93 (1.39)	0.44		0.044	0.40	0.018			0.40	810.0	0.18	0.047		4.726 4.621	5.094 5.047	5.112	5.112	5.262	0.150 3	3/12

amendments A ORIGINAL ISSUE FOR OPERATIONAL WORKS APPROVAL 27.08.11 PTY. LTD.	"Ocean Breeze Estate"	SCALE (AT A1 SIZE)	HOR N.T.S.	DRAWN DESIGNED	J.P.
CIVIL ENGINEERING DESIGN AND DRAFTING 6 Neptune Court Ph. (07) 4036 1690 Mt. Sheridan Q 4868 Mob. 0408 770 394	STAGE 4A OF PROPOSED RESIDENTIAL SUBDIVISION AT JULAJI CLOSE, COOYA BEACH	DATE	JUNE 2011	CHECKED	J.P.
Emall: ʃimpapas@westnet.com.au	DRAWING TITLE: STORMWATER DRAINAGE CALCULATIONS SHEET	DWG NUMBE	R 1208 -	- C13 A	AMDT A